
**Name of Candidate:** Timur Ermatov  
**PhD Program:** Physics  
**Title of Thesis:** Optical properties of hollow-core microstructured fibers modified by polymers and/or inorganic nano- and submicron particles  
**Supervisor:** Professor Dmitry Gorin

**Name of the Reviewer:** Sakellaris Mailis

<table>
<thead>
<tr>
<th>I confirm the absence of any conflict of interest</th>
<th>Date: 28-09-2021</th>
</tr>
</thead>
<tbody>
<tr>
<td>(Alternatively, Reviewer can formulate a possible conflict)</td>
<td></td>
</tr>
</tbody>
</table>

The purpose of this report is to obtain an independent review from the members of PhD defense Jury before the thesis defense. The members of PhD defense Jury are asked to submit signed copy of the report at least 30 days prior the thesis defense. The Reviewers are asked to bring a copy of the completed report to the thesis defense and to discuss the contents of each report with each other before the thesis defense.

If the reviewers have any queries about the thesis which they wish to raise in advance, please contact the Chair of the Jury.

**Reviewer’s Report**

Reviewers report should contain the following items:

- Brief evaluation of the thesis quality and overall structure of the dissertation.
- The relevance of the topic of dissertation work to its actual content
- The relevance of the methods used in the dissertation
- The scientific significance of the results obtained and their compliance with the international level and current state of the art
- The relevance of the obtained results to applications (if applicable)
- The quality of publications

The summary of issues to be addressed before/during the thesis defense
The thesis authored by Timur Ermatov is investigating the topic of modifying microstructured optical fibres (MOFs) to tune their optical properties and to functionalize them for sensing applications. The candidate has successfully deposited various organic and inorganic substances onto the inner wall of hollow core MOFs and demonstrated the changes in the spectral transmission along with sensing performance.

The thesis represents a substantial amount of, mainly experimental, work that yielded excellent results, as demonstrated by the rich research output in terms of publications and conference contributions. The candidate has published six papers in four of which is the first author, including a review article, and is a co inventor in three patent applications. Furthermore, the majority of papers are published in high quality/impact photonic journals, which is evidence for the quality and novelty of the results.

The thesis represents a substantial contribution in the area of fibre sensing with notable results i.e. the multispectral optical sensing used to derive the refractive index of pure substances from measurements in solvents thus providing reference data for materials as well as real time concentration measurements.

The content of the thesis is in line with the intended work and the methods that have been used are appropriate for this research work.

The work is extremely relevant to applications in the area of bio medical sensing using microstructured optical fibres. This is evident from the number of patents that stem from this work.

The draft of the thesis that was available to me for review was not however free from imperfections and can be definitely improved. I have therefore chose the second option in the provisional recommendation that calls for revisions. These revisions are outlined below and are listed in an annotated version of the thesis.

A summary of general remarks for the improvement of the thesis by Mr Ermatov is given here.

- The introductory part to the thesis, and to some of the chapters requires reorganization as well as additional components.
- The section on the outlook of the research is actually missing. The conclusion and outlook part must be rewritten to reflect the prospects of the research outcomes.
- There are several presentational deficiencies that have been identified.

A detailed list of the required revisions are included in the annotated version of the thesis that I am submitting along with this document.

Provisional Recommendation

☐ I recommend that the candidate should defend the thesis by means of a formal thesis defense.
I recommend that the candidate should defend the thesis by means of a formal thesis defense only after appropriate changes would be introduced in candidate’s thesis according to the recommendations of the present report.

The thesis is not acceptable and I recommend that the candidate be exempt from the formal thesis defense.
OPTICAL PROPERTIES OF HOLLOW-CORE MICROSTRUCTURED FIBERS MODIFIED BY POLYMERS AND/OR INORGANIC NANO- AND SUBMICRON PARTICLES

Doctoral Thesis

by

TIMUR ERMATOV

DOCTORAL PROGRAM IN PHYSICS

Supervisor
Professor Dmitry Gorin

Moscow - 2021

© Timur Ermatov 2021
I hereby declare that the work presented in this thesis was carried out by myself at Skolkovo Institute of Science and Technology, Moscow, except where due acknowledgement is made, and has not been submitted for any other degree.

Candidate (Timur Ermatov)
Supervisor (Prof. Dmitry Gorin)
Abstract

This work presents a study of the fabrication and the experimental and theoretical characterization of functionalized hollow-core microstructured optical fibers (HC-MOFs). It was accomplished in the scope of a doctoral thesis at the Skolkovo Institute of Science and Technology in Moscow.

HC-MOFs provide a new means of exploiting the unique optical properties of hollow waveguides, such as a broad window of transmission extending far into the infrared, and the guidance in a low refractive index material. This is totally impossible in conventional optical fibers. At the same time, when filling the hollow capillaries of HC-MOFs with liquid or gas medium, the overlap of a dissolved or suspended sample with the light field is close to unity. Moreover, a series of post-processing techniques applied to the fibers improve their performance and gives a rise to new applications.

Within the framework of this thesis a comprehensive study of new experimental techniques that allow the controlled modification of the inner surface of fiber capillaries with nanofilms of various thicknesses and nature (polymer, organic, composite) using the highly controllable and reproducible layer-by-layer (LbL) assembly is introduced. The impact of the functionalization on the optical transmission of HC-MOFs has been investigated in a broad spectral range (400 – 1500 nm).

Following the emerging fields of biophotonics and optofluidics, the practical application of in-fiber multispectral optical sensing (IMOS) based on a set of functionalized HC-MOFs has been verified by advanced refractometric measurements of biological liquids on the example of bovine serum albumin (BSA) at different concentrations. Albumin is the most abundant circulating protein. The plasma albumin concentration is normally between 35 and 50 g L\(^{-1}\), while its deviations indicate various abnormal conditions and diseases. The performance of IMOS has been demonstrated by measuring the concentration of BSA dissolved in water and a phosphate-buffered saline solution in both static and dynamic modes and a resolution of \(~1\, \text{g L}^{-1}\) when determining the BSA concentration was shown, which matches the accuracy of standard tests on
albumin. Pushing the limits further, it might eventually be possible to retrieve detailed information on the investigated solutions \textit{in situ}.

The foundations of this thesis can be found throughout different fields of science and technology. Therefore, a brief introductory review of the relevant fields will be given.

A theoretical study based on the analytic treatment of resonant guidance in HC-MOFs as well as numerical simulations covering the evolution of transmission spectra followed by the functionalization of fiber capillaries provided a deeper insight into the guidance mechanism and helped the extraction of the thicknesses of deposited layers and the refractive indexes of the investigated solutions.
List of publications

Research articles


TE and RN have an equal contribution.


Main contribution.


Contribution: transmission spectra measurements of hollow-core microstructured optical fibers.

Main contribution.


Main contribution.


Contribution: transmission spectra measurements of hollow-core microstructured optical fibers.

**Review articles**


Main contribution.

**Patents**


3. Optoacoustic sensor based on structural optical fiber, application № 2020113886, in collaboration with Laboratory of Nanomaterials Skoltech, 2021.

Conference proceedings


Main contribution.

Participation in scientific conferences

1. 28th International Conference on Advanced Laser Technologies, 6 – 10 September 2021, talk with title “Optical properties of functionalized microstructured fibers and their sensing capabilities”, online format.


Table of Contents

ABSTRACT ............................................................................................................................................ 3

LIST OF PUBLICATIONS ....................................................................................................................... 5

TABLE OF CONTENTS ............................................................................................................................. 9

LIST OF SYMBOLS, ABBREVIATIONS .................................................................................................... 11

LIST OF FIGURES ................................................................................................................................... 12

LIST OF TABLES ...................................................................................................................................... 18

1. CHAPTER 1. INTRODUCTION ........................................................................................................... 19
   1.1 Motivation ......................................................................................................................................... 19
   1.2 Outline of this Thesis ...................................................................................................................... 22

2. CHAPTER 2. THEORETICAL BACKGROUND .................................................................................... 24
   2.1 Historical overview of fiber optics ................................................................................................... 24
   2.2 Maxwell equations ............................................................................................................................ 28
   2.3 Effective medium approximation theory ........................................................................................ 29
   2.4 Light guidance in conventional optical fibers ............................................................................... 30
   2.5 Fabrication of hollow-core microstructured optical fibers ............................................................ 31
   2.6 Physical demonstrative approach to the waveguiding properties of hollow fibers ....................... 34
   2.7 Light guidance in hollow-core microstructured optical fibers .................................................... 35
   2.8 Functionalization of optical fibers .................................................................................................. 37
   2.9 Polyelectrolytes ............................................................................................................................... 44
   2.8 Layer-by-layer assembly ............................................................................................................... 46
   2.9 Stimuli-responsive layer-by-layer complexes ................................................................................. 47
   2.10 1D photonic crystal based sensing .............................................................................................. 48
   2.11 Capillary condensation phenomena ............................................................................................. 49
   2.12 Opal-like photonic crystals .......................................................................................................... 50

3. CHAPTER 3. FUNCTIONALIZED OPTICAL FIBERS ......................................................................... 52
   3.1 Introduction ..................................................................................................................................... 53
   3.2 Motivation ..................................................................................................................................... 55
   3.3 Materials and Methods ................................................................................................................. 56
      3.3.1 HC-MOF samples ...................................................................................................................... 56
      3.3.2 Chemical reagents ................................................................................................................... 58
      3.3.3 Multilayered deposition process ............................................................................................... 59
      3.3.4 Optical transmission of functionalized MOFs ......................................................................... 60
   3.4 Results and Discussion .................................................................................................................... 61
      3.4.1 Morphology of PAH-PSS multilayers ...................................................................................... 62
      3.4.2 The structure of silica particle-based fiber coating ................................................................. 64
      3.4.3 Magnetite-based nanocoating for functionalization of microstructured optical fibers .......... 67
      3.4.4 Optical characterization of MOFs functionalized by polymer multilayers ............................. 68
      3.4.5 Optical characterization of MOFs functionalized by silica particles ..................................... 73
      3.4.6 Optical characterization of MOFs functionalized by composite multilayers ........................ 76

9
3.4.5 Demonstration of mid-IR guidance in designed HC-MOFs .............................................. 77
3.5 SUMMARY.......................................................................................................................... 79

4. CHAPTER 4. SILICA PARTICLES FUNCTIONALIZED PHOTONIC CRYSTAL
BASED SENSOR......................................................................................................................... 81

4.1 MOTIVATION .................................................................................................................. 81
4.2 EXPERIMENTAL SECTION ......................................................................................... 81
  4.2.1 The structure of the photonic crystal ................................................................. 81
  4.2.2 Calibration of fabricated structures ................................................................. 83
  4.2.3 Silica particles coating on the surface of photonic crystal ............................ 85
  4.2.4 Optical characteristics of water condensation on the sensor surface ................. 87
4.3 SUMMARY ..................................................................................................................... 89

5. CHAPTER 5. POSTMODIFICATION OF FUNCTIONAL NANOICOATING ........... 90

5.1 INTRODUCTION ........................................................................................................... 90
5.2 MOTIVATION .............................................................................................................. 90
5.3 EXPERIMENTAL SECTION ....................................................................................... 91
5.4 SUMMARY ................................................................................................................ 98

6. CHAPTER 6. IN-FIBER MULTISPECTRAL OPTICAL SENSING ............. 100

6.1 INTRODUCTION .......................................................................................................... 100
6.2 MOTIVATION ............................................................................................................. 100
6.3 RESULTS AND DISCUSSION ................................................................................... 102
  6.3.1 Empirical extraction of RI for liquid filling ....................................................... 102
  6.3.2 Transmission of HC-MOFs filled with a water-BSA solution ............................ 103
  6.3.3 IMOS in static mode ......................................................................................... 104
  6.3.4 Impact of the liquid sample internal losses on the HC-MOF transmission ......... 107
  6.3.5 Refractive index sensitivity and figure of merit .............................................. 108
  6.3.6 Optical dispersion of refractive index for bovine serum albumin ......................... 110
  6.3.7 IMOS in real-time .......................................................................................... 112
6.4 SUMMARY ................................................................................................................ 115

7. CHAPTER 7. NONCONTACT CHARACTERIZATION OF MICROSTRUCTURED
OPTICAL FIBERS COATING IN REAL-TIME ................................................................. 117

7.1 MOTIVATION ............................................................................................................. 117
7.2 RESULTS AND DISCUSSION ................................................................................... 118
  7.2.1 Experimental realization ................................................................................. 118
  7.2.2 In-situ monitoring of coating buildup ............................................................. 119
  7.2.3 In-situ monitoring of coating disintegration .................................................... 121
7.3 SUMMARY ................................................................................................................ 122

8. CONCLUSIONS AND FUTURE RESEARCH .................................................... 124

BIBLIOGRAPHY ............................................................................................................... 126
List of Symbols, Abbreviations

OF – optical fiber

MOF – microstructured optical fiber

HC – hollow-core

SC – solid-core

HC-MOF – hollow-core microstructured optical fiber

SC-MOF – solid-core microstructured optical fiber

IMOS – in-fibre multispectral optical sensing

LbL – layer-by-layer

TIR – total internal reflection

PE – polyelectrolyte

PCF – photonic crystal fiber

PAH – poly (allylamine hydrochloride)

PEI – polyethylenimine

PSS – poly (styrenesulfonate)

PDDA – poly (diallyldimethylammonium chloride)

BSA – bovine serum albumin

TA – tannic acid

SEM – scanning electron microscopy

RI – refractive index

NA – numerical aperture

CTC – circulating tumor cells
List of Figures

Figure 2-1: A beam of light is focused by a water-filled rectangular tank and onto an opening on the other side. The light is guided along the water jet by total internal reflection. ................................................................. 25

Figure 2-2: Light can leak from unclad fibers where they touch other objects. (b) Total internal reflection at the boundary between core and cladding guides light along a clad optical fiber. Adapted from [23]. ................................................................................................................. 26

Figure 2-3: Schematic of solid-core and hollow-core MOFs. ................................................. 27

Figure 2-4: (a) separated-grain structure and (b) aggregate structure depict two microstructures for heterogeneous two-phase media. .................................................................................. 30

Figure 2-5: Schematic of light guidance in step-index optical fibers. The full acceptance angle illustrates the maximum light cone which is allowed to propagate in the fiber structure. .......................................................................................................................... 32

Figure 2-6: Schematic of multimode (a) and single-mode (b) OFs. Color arrows indicate light different modes. Multimode fibers consist of a relatively large core (~ hundreds of microns) surrounded by a cladding layer. Single-mode fibers are featured a smaller core with a typical size of few microns so the only fundamental light mode can propagate along the whole fiber length while the higher-order modes are escaped in the cladding. 33

Figure 2-7: Schematic of the fabrication of microstructured optical fibers by the “stack-and-draw” method ........................................................................................................................................ 34

Figure 2-8: Cross- and longitudinal sections of the hollow (left) and tube (right) waveguides.................................................................................................................................................. 35

Figure 2-9: The SEM images of the fiber end face and the capillary wall of the first cladding ring. ........................................................................................................................................... 36

Figure 2-10: Theoretical vs experimental transmission for an unmodified and empty HC-MOF with a core diameter of 240 μm and the wall thickness for the first capillary layer of 1.8 μm [14]. ........................................................................................................................................ 37

Figure 2-11: Optical fiber sensor based on SPR. Illustration of the working principle of the fiber-based SPR sensor. The shift of the plasmon resonant wavelength is associated with the change in the refractive index of the sample (δn) defining the resonant condition [48].................................................................................................................. 38

Figure 2-12: An overview of different structure modified optical fibers. (I) Geometry-modified optical fibers: (a) unclad, etched, (b) side-polished, D-shaped fibers, (c) hetero-core structures, (d) U-shaped fibers and (e) arrayed fiber end face. (II) Grating-assisted fibers. (III) Specialty fibers [46]. ........................................................................................................................................ 39

Figure 2-13: The illustration of the concept of label-free optical biosensor [60].............. 40

Figure 2-14: The sketch of the functionalized fiber surface showing the binding of anti-EGFR antibody conjugated SERS nanotag to the cancer protein (positive human epithelial carcinoma cells A431) immobilized on the inner wall of the core of MOF [61]. ........................................................................................................................................ 41

Figure 2-15: Schematic of layer-by-layer assembly of inversely charged polyelectrolytes onto the planar substrate. The immersion with water solution in between the deposition
cycles ensures the elimination of unbounded particles. The deposition cycles are repeated until the desired number of layers is achieved.

Figure 2-16: The Otto configuration uses a bulk plasmonic material separated from the prism by a thin layer of a dielectric analyte. In the Kretschmann configuration, the plasmonic material is deposited as a thin film on the prism, with the dielectric analyte on top. In both cases, the prism is used to match the wavevector of the incident light to the wavevector of the surface plasmon polariton at the interface between the dielectric analyte and plasmonic material. Adapted from [125].

Figure 2-17: Schematic outlining the interaction of light with the periodic material (opal-like photonic crystal) with an effective refractive index, and the light scattered by the sphere planes. $\theta_1$ and $\theta_2$ are the angles between the normal to the sample surface and the direction of the incident and refracted light beams, respectively; $n_{\text{eff}}$ and $n_1$ is the effective refractive index of the photonic crystal and the external medium, respectively. Adapted from [129].

Figure 3-1: SEM images of the HC-MOF used in the experiments. (a) General view. (b) Inset showing the wall thickness of the central capillary.

Figure 3-2: Optical dispersion of the fiber glass.

Figure 3-3: Chemical structure of the polyelectrolytes used for the creation of functional coatings (PAH - poly (allylamine hydrochloride), PSS - poly (styrene sulfonate), PDDA - poly (diallyldimethylammonium chloride) and PEI - polyethylenimine).

Figure 3-4: The setup for functionalization of HC-MOFs with LbL assembly. A peristaltic pump drives the flow of applied solutions (polyelectrolyte water solution, silica particles colloid solution, magnetite particles colloid solution and pure water) through the full fiber length, leading to the formation of the polymer coating on the inner surface of the core capillary. The procedure is repeated to create the desired number of bilayers. The insets depict the scanning electron microscopy (SEM) images of the fiber end face. Adapted from [14].

Figure 3-5: Schematics of the transmission measurement setup. 10X states for the 10X Olympus objectives.

Figure 3-6: Polymer coating thickness versus the number of PE bilayers. The thickness is fitted to obtain the coincidence of the minima positions for both the experimental and calculated transmission spectra. Error bars show the coating roughness. Adapted from [14].

Figure 3-7: Comparison of the experimental fiber transmission spectra with the theoretical ones obtained by adjusting the thickness of the polymer coating (60 nm per 40 polymer bilayers) [14].

Figure 3-8: SEM images of MOF end faces and magnified capillary surfaces. (a) MOF sample after deposition of one layer of 300-nm silica particles. (b) MOF sample after deposition of one layer of 420-nm silica particles [94].

Figure 3-9: SEM images of MOF end face (a) and magnified capillaries (b,c) with one deposited layer of 900-nm silica particles [94].

Figure 3-10: (a) SEM image of MOF end face; (b,c,d) magnified SEM images of capillaries with one, two and three deposited layers of 300-nm silica particles, respectively [94].
Figure 3-11: SEM image of MOF capillaries with two layers of 300-nm SiO$_2$ nanoparticles for the cases of (a) PDDA/PSS/PDDA and (b) PDDA intermediate layers, respectively at different magnifications top and bottom [94].

Figure 3-12: (a) SEM image of MOF end face with the highlighted region of the inner surface of the hollow-core. (b,c) Magnified regions of the capillary walls illustrating the formation of composite nanocoating on the example of MOF samples modified with (b) 13 PAH/MNPs bilayers and (c) 28 PAH/MNPs bilayers [142].

Figure 3-13: Optical characterization of HC-MOFs functionalized by PEs adsorbed from the salt-free buffer (see Fabrication chapter). (a,b) Transmission spectra in the visible (400 nm – 900 nm) and near-infrared (900 nm – 1500 nm) ranges. The results for 6 samples with various numbers of PE bilayers are presented. Note the different scales along the x-axis for (a) and (b). Shifts of maxima (c) and minima (d) of the transmission along with the linear fits. Adapted from [14].

Figure 3-14: Optical characterization of HC-MOFs functionalized by PEs dissolved in saline buffer (0.15 M NaCl). (a) Transmission spectra in the visible range. The results for 6 samples with a different number of PE bilayers are presented. Shifts of maxima (b) and minima (c) of the transmission along with the linear fits [14].

Figure 3-15: Characterization of optical losses in functionalized HC-MOFs by the cut-back technique. (a) Unmodified MOF. Fibers coated with 14 (b) and 40 (c) PE bilayers in the salt-free solution. Shadow areas show the error range. (d) The minimal optical loss in the transmission windows as a function of the bilayer quantity. Adapted from [14].

Figure 3-16: Spectral shift of local transmission bands for MOF samples with one deposited layer of 300-nm and 420-nm SiO$_2$ particles into MOFs with an internal buffer layer [94].

Figure 3-17: Transmission spectrum of MOF sample with one deposited layer of 900-nm silica particles (blue). MOF spectrum with a buffer layer (red) [94].

Figure 3-18: Transmission spectra for MOFs coated with the buffer layer only (red) and with one (blue), two (black) and three (green) layers of 300-nm SiO$_2$ particles [94].

Figure 3-19: (a) Comparison on transmission spectra of non-modified and modified MOFs. (b) The spectral shift of the maximum transmission spectrum located at 550 nm induced by the deposition of composite nano-coating on the inner surface of MOF hollow-core. The dashed line shows the linear fit of the experimental points. The error bars correspond to the spectrometer's optical resolution. Adapted from [142].

Figure 3-20: (a) Fiber loss of non-modified (empty) MOF sample. (b,c) The loss estimation of MOF samples modified with (b) 11 and (c) 23 PAH/ MNPs (Fe2O3). Adapted from [142].

Figure 3-21: Demonstration of broadband VIS – mid-IR light guidance. Blue curve states for the transmission spectrum of investigated MOFs, the shaded region illustrates the estimated loss interval summarizing the results of 4 samples of MOFs. The red dotted line is the calculated spectrum referred to the positions of minima in MOFs transmission [8].

Figure 4-1: The scheme of the photonic crystal providing the resonance at 780 nm. 

Figure 4-2: Schematic representation of the experimental setup.
Figure 4-3: Reflectance spectra of 8 fabricated PC samples. The same shape denotes equal sensitivity of the samples. ................................................................. 84
Figure 4-4: Area of analyte condensation between 180 nm particles and substrate (under normal conditions). ................................................................. 85
Figure 4-5: Schematic of dip-coating technique. ................................................................. 86
Figure 4-6: SEM images of photonic crystal surface prepared by the dip-coating method: (a) – hydrophilic and (b) - hydrophobic......................................................... 87
Figure 4-7: Experimental gas circulation setup. ................................................................. 87
Figure 4-8: Dependence of reflection on an angle for (a) – hydrophilic and (c) – hydrophobic coatings. ......................................................................................... 88
Figure 5-1: Evaluation of the coating roughness and thickness. (a) and (b) The structure of 8 BSA/TA bilayers before and after the alkaline treatment across the fiber cross-section. (c) The structure of 18 BSA/TA not-etched bilayers along the fiber. The frame color corresponds to the position where the SEM images were taken. The initial length of all the fibers was 6 cm, then three equidistantly located cuts were taken. ................. 92
Figure 5-2: Characterization of the BSA/TA coating. (a) SEM micrographs of BSA/TA multilayers (indicated by the pseudocolor) before and after the etching. The coating (b) thickness and (c) roughness before etching as a function of the number of bilayers. The coating (d) thickness and (e) roughness versus the treatment time. The coating thickness is evaluated from SEM images (bars) and the shifts in the fiber transmission windows (red points). Error bars denote the coating roughness. The linear fit in (b) corresponds to the thickness of 5.2 nm per single bilayer. The coating roughness in (e) is fitted by the exponential function with the initial roughness $R0 = 25.9$ nm and the decay time $\delta t = 2.2$ min. ......................................................................................................................... 93
Figure 5-3: Coating roughness vs coating thickness................................................................. 95
Figure 5-4: Evolution of the fiber transmission spectrum (a) with growth in the number of BSA/TA bilayers deposited and (b) in time upon the alkaline treatment for the HC-MOF coated with 28 BSA/TA bilayers. Relative shifts of the transmission maxima vs (c) the number of BSA/TA bilayers deposited and (d) the treatment time for the initial coating with 28 BSA/TA bilayers. The measured values are denoted by points joined with lines as guides for the eye................................................................. 96
Figure 5-5: Optical fiber loss as a function of (a) treatment time and (b) coating thickness. Fiber losses are calculated by averaging across minimal losses for all transmission windows, and the error bars correspond to the standard deviation. The substrate with 28 initial BSA/TA bilayers was etched. The fiber optical loss in (a) is fitted by the exponential function with the initial fiber loss $\alpha0 = 1.16$ dB cm$^{-1}$ and the decay time $\delta t = 4.1$ min. The loss measurements were performed by the cut-back technique. ....... 98
Figure 6-1: Theoretical and experimental transmission spectra of HC-MOF filled with water and the BSA-water solution at the concentration of 20 g L$^{-1}$ [14]. ......................... 103
Figure 6-2: Static measurements of the transmission for HC-MOFs filled with a water-BSA solution. (a) The schematic of the optical setup. (b) The transmission of liquid-filled HC-MOF for different concentrations of BSA [14]. ......................................................... 104
Figure 6-3: Performance of IMOS for BSA dissolved in deionized water in static mode. (a) Transmission spectrum evolution with increasing BSA concentration for the non-
modified HC-MOF. (b) Optical dispersion of BSA in a water buffer with different concentrations. The colored points indicate the RI values extracted from the shifts in the minima and the peak centroids of the fiber transmission spectra, and the solid lines mark their Sellmeier fits. For pure water, the Sellmeier fit describes the water dispersion adopted from Ref. [186]. The error bars are obtained from the spectrometer's optical resolution. The stars mark RIs measured by the Abbe refractometer, provided for comparison [14].

Figure 6-4: Algorithm for the extraction of optical dispersion of BSA solution at different concentrations.

Figure 6-5: Calibration relating the concentration of BSA and RIs of the BSA-water solution at different wavelengths. The RIs of BSA are extracted from the Sellmeier fits of the experimental points [14].

Figure 6-6: Fibre transmission spectra for a various imaginary part of the sample refractive index: 0 (black), 0.0005 (cyan), 0.001 (blue), 0.005 (red) and 0.01 (magenta). The real part of RI equals to 1.33 [14].

Figure 6-7: (a,b,c,d) The minima positions extracted from the transmission spectra of HC-MOFs as a function of the filling refractive index obtained by variations in the concentration of BSA. The error bars are smaller than the data points [14].

Figure 6-8: The refractive index of BSA determined via the Maxwell Garnett approximation. Points correspond to the measurements of RI for BSA-water, and solid lines mark the Sellmeier fits. The extraction was performed for 3 concentrations of BSA to show the repeatability of the result [14]. The error bars are smaller than the marker size. The stars mark BSA RI values adopted from Refs. [187–191,193].

Figure 6-9: The refractive index of BSA extracted via the Maxwell Garnett approximation. Circles correspond to the measurements of RI for the BSA supplied by Sigma-Aldrich (>96% purity) and triangles to the BSA supplied by Agat-Med (50% purity), and solid lines mark the Sellmeier fits. The extraction is performed for 3 concentrations of BSA to show repeatability of the result [14]. The pentagrams mark BSA RI extracted from Refs [187–190,193,199].

Figure 6-10: Schematic of the custom-designed liquid cells. Dimensions are denoted in mm [14].

Figure 6-11: Illustration of the dynamic multispectral sensing concept for liquid samples. Scheme of the setup for transmission characterization of HC-MOFs. Fiber facets are fastened in liquid cells (LCs), which are optically accessible via thin glass windows, allowing simultaneous pumping of fluids through fiber capillaries and measurement of the transmission spectrum. The red rays illustrate the light path from a broadband halogen lamp through the HC-MOF to the spectrometer and the CCD (charge-coupled device) camera to record the output mode profile. The insets depict the input and output spectra for different concentrations of BSA dissolved in PBS [14].

Figure 6-12: IMOS in real-time for BSA dissolved in PBS buffer. The colored lines denote instantaneous positions of the transmission minima when the peristaltic pump is switched between 5 solutions with different concentrations of BSA. The black lines exhibit the data smoothed with MATLAB. The flow rate created by the peristaltic pump is fixed at 1 mL min⁻¹ [14].
Figure 6-13: Illustration of the automatic fiber switching in the system optical path by a piezo stage. Independent optical paths can be created to perform measurements simultaneously with all fibers [14].

Figure 7-1: (a) Comparison of the experimental and theoretical transmission spectra for the water-filled non-modified and coated by the PEs dissolved in a buffer containing 0.15 M NaCl HC-MOF. The theoretical plot was obtained by adjusting the thickness of the polymer coating as 18 nm per 3 PAH/PSS bilayers. (b) The spectral evolution of the transmission minima associated with LbL assembly. The colour lines indicate instantaneous positions of the transmission minima when the peristaltic pump is switched between PE solutions and deionized water (w). The black lines exhibit the data smoothed with MATLAB.

Figure 7-2: SEM micrographs of the core capillaries functionalized with 3 PAH/PSS bilayers in the presence of (a) 0.5 and (b) 0.15 M NaCl, respectively. (c) Coating thickness vs the number of PE bilayers. The coating thickness is evaluated from the shifts in the fiber transmission windows (points). Lines correspond to the thickness of 5.8 nm (0.15 M NaCl) and 10.6 nm (0.5 M NaCl) per single bilayer.

Figure 7-3: (a) SEM micrographs of the uncoated fiber and the fiber functionalized with BSA/TA multilayers followed by the alkaline treatment. (b) In situ monitoring of the BSA/TA coating disintegration (black and red line – 4 BSA/TA bilayers upon the treatment by pH 9 and 11, respectively. Blue – 8 BSA/TA bilayers treated by pH 11. The green line indicates the start of the alkaline treatment.
List of Tables

Table 2-1: Summary of the MOF functionalization techniques and their potential applications [10]......................................................................................................................................................... 43
Table 3-1: Transmission peaks shift of MOF samples with one deposited layer of 300-nm and 420-nm SiO$_2$ particles [94].............................................................................................................................................. 74
Table 3-2: Spectral shift of local transmission bands for MOF samples with multiple deposited silica particle layers. The diameter of silica particles is 300-nm [94]........... 76
Table 3-3: Comparison of the optical performance of reported microstructured optical fibers [8]................................................................................................................................................. 79
1. Chapter 1. Introduction

1.1 Motivation

Since its inception in 1996 [1], microstructured optical fibers (MOFs) have been widely developed followed by the realization of advanced coatings on both the inner and outer fiber surface. In contrast to all-solid optical fibers (OFs) made of silica and its counterparts, the structure of MOFs forming by a complex array of air channels allows the fabrication of single-material fibers with a high air-filling fraction (>90%) [2,3] giving a rise to the appearance of separate classes of optical waveguides called hollow-core and solid core MOFs (HC-MOFs and SC-MOFs) [4]. Traditionally, conventional optical fibers are extensively used in various fields of photonics, communications, and remote sensing [5]. The realization of light guidance in the air-filled core, in turn, enables the strong interaction between an injected medium and the light mode that opens new perspectives for the applications of holey OFs, which are not possible with all-solid fibers. In particular, several technological breakthroughs such as the low-loss light guidance, guidance only the fundamental mode at all frequencies, supercontinuum generation and the transmittance in near- and middle-IR spectral ranges were reported for HC-MOFs [6–8].

The other important advantage of HC-MOFs is the accessibility of the fiber air channels for molecular and nanoscale functionalization that brings application-oriented functionalities into fibers in fields such as optics, biophotonics and healthcare [9,10]. Moreover, functional nanocoatings of HC-MOFs have extended the domain of their applications to biosensing and photochemistry [11]. This includes the immobilization of plasmonic nanoparticles for Raman-assisted detection, antibody/antigen biosensing and
optofluidic refractive index (RI) sensing [12–15]. Moreover, naturally-derived materials can be also incorporated into the self-assembled multilayers where nontoxic or even biocompatible materials are needed [16].

Besides, HC-MOFs represent an attractive playground for the creation of in-fiber optical sensors featuring the strong interaction between a guided mode and an analyte in the test [11]. The state of the art in optical biosensing is focused on reaching high sensitivity at a single wavelength by using any type of optical resonance. They include collective resonances in plasmonic and dielectric metasurfaces [17,18], plasmon polaritons in hyperbolic metamaterials [19] and many others [20]. Although some of these structures can support several resonances (typically less than 4), the single resonance is taken for sensing, providing a maximum figure of merit and refractive index sensitivity. This common strategy, however, overlooks an interesting and promising possibility of simultaneous measurements of a bioanalyte’s refractive index in a wide range of wavelengths that can act as a simple and cost-effective fingerprint of liquid biosamples providing crucial information about real-time variations in their composition without expensive and complex functionalization of sensing template nanostructures with antibodies, aptamers and other analyte binders. For this reason, the technique that allows the fast, precise and easy sensing of biological liquids in the broad spectral range is highly desirable and is a central part of this thesis [14].

Throughout this work, the author makes significant advances towards resolving this issue by introducing the method of in-fiber multispectral optical sensing (IMOS) for both the static and dynamic refractometric measurements of biological liquids. The operation
principle is based on detecting spectral shifts of multiple Fabry-Perot resonances in the core capillary wall of several functionalized HC-MOFs with slightly shifted transmission windows when a liquid sample is streamed through it via specially designed liquid chambers.

It is worth to mention, that regardless of the various experimental techniques applied for the creation of functional coatings on the fiber surfaces, no detailed characterization of transmission losses in functionalized fibers has been published yet. However, novel modalities typically come with increased optical losses since a significant surface roughness of functional layers gives rise to additional light scattering, restricting the performance of functionalization. Another problem is that the conventional strategies rely on using materials with poor biocompatibility and high toxicity which are not optimal for sensitive in vivo applications.

To solve this issue, the author introduces a novel type of biocompatible and removable nanocoating for HC-MOFs formed by layer-by-layer assembly of stimuli-responsive organic materials resulting in decreasing the coated fiber optical losses by three times. Additionally, the creation of a reusable MOF-based biosensor has been demonstrated in the example of organic multilayers deposited on the inner fiber surface.

The following chapters will try to give a detailed study of the functionalized HC-MOFs, discussing the possibilities and limitations of hybrid waveguide fabrication and presenting a series of optical experiments that illustrate practical usage and realization of the produced structures.
1.2 Outline of this thesis

After a brief introduction to the topic (chapter 1), the theoretical background required for a fundamental understanding of the reported questions is given in Chapter 2, including waveguide theory of the conventional step-index fibers based on total internal reflection phenomenon and microstructured optical fibers features the light guidance in low refractive index materials. Chapter 2 continues with a brief description of the most widely used techniques used for the functionalization of optical fibers emphasizing the key characteristics of layer-by-layer (LbL) assembly. One-dimensional (1D) and opal-like photonic crystals are discussed at the end of Chapter 2.

Chapter 3 is addressed a series of experimental fabrication techniques applied for the surface modification of fiber capillaries. They rely on the electrostatic attraction of inversely charged polyelectrolytes and hydrogen bonding and hydrophobic interactions of organic nanoparticles, and also entropy factor plays a significant role. The fabrication chapter includes a study of coating growth depending on various assembly conditions and the analysis of transmission losses induced by deposited structures. Additionally, post-processing techniques applied to the coated fibers are discussed in Chapter 5 on the example of pH-responsive organic films.

Chapter 4 is devoted to the experimental realization of the porous functional layer on the top of the sensitive surface of the 1D photonic crystal. The practical realization of the designed sensor structure has been demonstrated for the monitoring of the relative humidity change.
Chapter 6 dedicated the "proof-of-concept" work that presented the real-life application of functionalized HC-MOFs for multispectral refractometric measurements of biological liquids at different concentrations. All the experiments are done at both static and dynamic regimes.

Chapter 7 gives a short conclusion and the statement of primary outcomes along with the possible future applications based on functionalized MOFs.
2. **Chapter 2. Theoretical background**

In this chapter, the theoretical background required for a fundamental understanding of the topics presented in this thesis is introduced. A detailed discussion or derivation of the equations is beyond the scope of this work. A comprehensive description of electromagnetic theory and light-matter interaction can be found in textbooks such as [18, 19, 20].

2.1 **Historical overview of fiber optics**

The birth of modern fiber optics is associated with the discovery of the phenomenon of total internal reflection (TIR) for the light traveling at the border of two media that has been shown by Johannes Kepler, a German mathematician and astronomer, in 1611, ten years before Willebrord Snell derived his famous formula for the refraction of light [21].

One of the first experimental realizations demonstrating that light can be confined and guided inside a transparent curved medium goes back to the year 1842, when Jean-Daniel Colladon, a 39-year-old professor at the University of Geneva, published an article “On the reflections of a ray of light inside a parabolic liquid stream” [22]. He wanted to show fluid flow through various holes and the breaking up of water jets observed earlier by French physicist Felix Savart [23]. When the light rays in the water hit the edge of the jet at a glancing angle, TIR trapped them in the liquid (Figure 2.1).
Figure 2-1: A beam of light is focused by a water-filled rectangular tank and onto an opening on the other side. The light is guided along the water jet by total internal reflection.

However, the first practical application of optical fibers was demonstrated almost one hundred years later in the form of fiber bundles without a cladding layer for medical imaging or endoscopy [24,25]. However, light can easily leak from unclad fibers where they touch other objects (Figure 2.2a). The use of different materials for waveguiding kept advancing the field over the decades, followed by the idea of embedding the high-index fiber core in a low-index glass cladding arose during the development of the first gastroscope by Lawrence Curtiss (Figure 2.2b) [23].
Nevertheless, even after the advent of lasers in the early 1960s, the use of optical fibers for long-distance data transmission did not appear practicable since the optical losses of glasses were still too high for telecommunication purposes. It was Charles Kao and George Hockham [26] who theoretically analyzed which structural and material requirements needed to be fulfilled to reduce losses in silica giving rise to modern fiber optics, and earning Kao the Nobel prize in Physics in 2009 [27].

A major step in the field of fiber optics was the invention of microstructured optical fibers by Philip Russell, demonstrated experimentally in 1996 on the example of solid-core MOFs whose structure is defined by an array of air-channels, running through the whole fiber length [1] (Figure 2.3). The idea to guide light by means of a photonic crystal cladding is based on the concept of photonic crystals proposed by Reinhard Ulrich [9], Philip Russell

![Schematic of solid-core and hollow-core MOFs.](image)

Figure 2-3: Schematic of solid-core and hollow-core MOFs.

HC-MOFs represent a separate class of optical waveguides, in which confinement of transmitted light is ensured by a complex array of air-capillaries surrounding the central hollow core. In such structures, light guidance can be achieved by two different methods, both, however, avoiding the need for total internal refraction [29]. First is the two-dimensional photonic bandgap mechanism, which allows tight optical confinement and transmittance of the light inside HC and prevents its escape into the photonic-crystal cladding. These structures refer to hollow-core photonic bandgap fibers (PBGFs) and lie within the scope of photonic-crystal fibers (PCFs). The central light-guiding HC surrounded by a thin glass wall (50–150 nm) supports the transmission of a tiny wavelength band with low loss over the whole waveguide length [3,30]. Another method is based on an anti-resonant reflecting optical waveguide structure. These are so-called hollow-core anti-resonant fibers (or inhibited-coupling fibers) [3]. They, in turn, do not allow the realization of photonic bandgap guidance because the glass wall thickness (typically hundreds of nanometers) is thicker than that required for broadband or multiband PBGFs. Nevertheless, featuring the relatively low loss operation over the broad wavelength range,
hollow-core anti-resonant fibers can further enhance the capability of HC-MOFs in various applications [8].

### 2.1 Maxwell equations

Light propagation in periodic complex structures has aroused considerable interest in the past few years. This interest was largely stimulated by Yablonovitch and co-workers who suggested that diffraction by periodic structures might lead to a ‘photonic insulator’ or photonic bandgap in which light is forbidden to propagate in a certain range of frequencies [31]. Maxwell’s equations, in turn, describe the generation and propagation of electromagnetic waves and relate the corresponding fields (∇⃗E(⃗r, t), ∇⃗H(⃗r, t)) to their sources (current density (j (⃗r, t) and charge density ρ(⃗r, t)), depending on space ⃗r and time t [32]. In their final form, they were developed by James Maxwell in 1865 [21] and combine Gauss’s laws, Faraday’s law of induction and Ampere’s law including the time-derivative of the displacement vector ∇⃗D. Maxwell’s equations in SI units are typically written as a set of four linear partial differential equations (Eqs. 2.1 – 2.4):

\[
\begin{align*}
\nabla \times \vec{E}(\vec{r}, t) &= -\frac{\partial}{\partial t} \vec{B}(\vec{r}, t) \\
\nabla \times \vec{H}(\vec{r}, t) &= -\frac{\partial}{\partial t} \vec{D}(\vec{r}, t) + \vec{j}(\vec{r}, t) \\
\n\nabla \cdot \vec{D}(\vec{r}, t) &= \rho(\vec{r}, t) \\
\n\nabla \cdot \vec{B}(\vec{r}, t) &= 0
\end{align*}
\]

where \( \rho \) is the external charge density, \( \vec{j} \) corresponds to the macroscopic current density, \( \vec{D} \) and \( \vec{B} \) are electric displacement and magnetic flux density (or magnetic induction), respectively.
In a vacuum, the fields $\vec{D}$ and $\vec{E}$, and $\vec{B}$ and $\vec{H}$, respectively, are related through (Eqs. 2.5 – 2.6):

\begin{align*}
\vec{D} &= \varepsilon_0 \vec{E} \quad (2.5) \\
\vec{B} &= \mu_0 \vec{H} \quad (2.6)
\end{align*}

In SI unit, $\varepsilon_0 = 8.8542 \times 10^{-12}$ F m$^{-1}$ is the vacuum permittivity and $\mu_0 = 4\pi\times10^{-7}$ H m$^{-1}$ is the vacuum permeability which has a relationship with the vacuum speed of light as (Eq. 2.7):

\[ c = \frac{1}{\sqrt{\varepsilon_0 \mu_0}} \quad (2.7) \]

In optics, we can assume $\vec{j} = 0$ and $\rho = 0$. For non-magnetic media, the magnetism is so weak that $\mu \approx 1$.

### 2.2 Complex refractive index

The materials used in this work are isotropic, non-magnetic and free of charges, leading to the following assumptions: $\varepsilon$ is scalar, $\vec{j} = 0$, $\rho = 0$ and for non-magnetic media, the magnetism is so weak that $\mu \approx 1$.

The refractive index $n$ of a medium can then be defined as a function of $\varepsilon$ and $\mu$ (Eq. 2.8):

\[ n = \sqrt{\varepsilon \mu} = n_{real} + in_{imaginary} \quad (2.8) \]

where the real part, $n_{real}$, shows the ratio of the velocity of light in vacuum and the velocity of light in the medium, and the imaginary part, $n_{imaginary}$, is the extinction coefficient, related to the material absorption in a medium.
2.3 Effective medium approximation theory

Effective medium approximation (EMA) theory aims to approximate a complex electromagnetic medium such as a colloidal solution of micro- and nanoparticles in water with a homogeneous effective medium [33]. The EMA mixing formulas give the permittivity of this effective medium in terms of the permittivities and volume fractions of the individual constituents of the complex medium [33]. Two different cases might be highlighted in the framework of EMA theory. The first is when one of the components can be considered as a host in which inclusions of the other components are embedded (Figure 2.4a), whereas the second is more appropriate to microgeometries where the grains of the various components are symmetrically distributed, with no clear matrix component [34] (Figure 2.4b).

![Separated-grain structure](image1)

![Aggregate structure](image2)

*Figure 2.4:* (a) separated-grain structure and (b) aggregate structure depict two microstructures for heterogeneous two-phase media.

These two approximations have been frequently used for investigating the properties of isotropic two-component mixtures, in which the components are isotropic materials with scalar dielectric coefficients and the components grains are assumed to be...
spherical. However, with simple generalization, EMA has been also adapted for isotropic mixtures including randomly oriented ellipsoidal grains [34].

Numerous expressions have been proposed to describe effective permittivity ($\varepsilon_{\text{eff}}$) in terms of the microstructural parameters and the dielectric functions of the constituents. The Maxwell Garnett mixing formula (Eq. 2.9) used for the cases when the volume fraction of the “host” or “environment” is much larger than that of the “inclusions”.

$$
\varepsilon_{\text{eff}} = \varepsilon_e + \varepsilon_e \frac{f_i}{1 - f_i} \frac{\frac{1}{N_x} \varepsilon_{\text{eff}} - \varepsilon_e}{\varepsilon_{\text{eff}} + \frac{N_y}{N_x} \varepsilon_{\text{eff}} - \varepsilon_e}.
$$

(2.9)

where $\varepsilon_e$ and $\varepsilon_i$ are the permittivities of the environment or host medium and the inclusions, respectively, $f_i$ is the volume fraction of the inclusions, and $N_x$, $N_y$ and $N_z$ are the depolarization factors over the x, y and z axes, respectively.

Bruggeman formalism (Eq. 2.10), in turn, is symmetric with respect to all medium components and does not treat any one of them differently. There is no more host-versus-guest hierarchy.

$$
(1 - f_1) \frac{\varepsilon_2 - \varepsilon_{\text{eff}}}{\varepsilon_2 + 2 \varepsilon_{\text{eff}}} + f_1 \frac{\varepsilon_1 - \varepsilon_{\text{eff}}}{\varepsilon_1 + 2 \varepsilon_{\text{eff}}} = 0
$$

(2.10)

where $\varepsilon_1$ and $\varepsilon_2$ are permittivities of the 1$^{\text{st}}$ and 2$^{\text{nd}}$ compounds of the mixture, and $f_1$ is the volume fraction of the 1$^{\text{st}}$ compound.

### 2.4 Light guidance in conventional optical fibers

In the most general case, the light guidance is achieved by the proper choice of fiber materials: a fiber core is made with a material whose refractive index is slightly higher than that of the surrounding cladding. For a step-index fiber, the light guidance can be explained using the model of the total internal reflection of light beams at the border between core and cladding zones (Figure 2.5).
One easily concludes that total internal reflection at the interface occurs if the external beam angle $\theta$ (in the air) fulfills the condition (Eq. 2.11):

$$\sin \theta = \frac{n_{cladding}}{n_{core}}$$  \hspace{1cm} (2.11)

where $\theta$ is the external beam angle, and $\sin \theta$ is also called numerical aperture of the fiber (NA), $n_{cladding}$ and $n_{core}$ state for the RI of the fiber cladding and core, respectively.

For the comparatively large sizes of the fiber microstructure, the treatment of the light propagation in terms of geometrical optics gives reasonable results (strongly multimode fibers) but is invalid for single-mode fibers consisted of smaller cores, where we should consider the wave nature of light (Figure 2.6).
Figure 2-6: Schematic of multimode (a) and single-mode (b) OFs. Color arrows indicate light different modes. Multimode fibers consist of a relatively large core (~hundreds of microns) surrounded by a cladding layer. Single-mode fibers are featured a smaller core with a typical size of few microns so the only fundamental light mode can propagate along the whole fiber length while the higher-order modes are escaped in the cladding.

The more detailed study of light propagation in optical fibers requires considering a wave phenomenon of light as well. A comprehensive description of the beam propagation method can be found in textbooks such as [35].

2.5 Fabrication of hollow-core microstructured optical fibers

The extensive development of HC-MOFs was driven by a novel fabrication method called the “stack-and-draw” technique. The technique was first introduced by Philip Russell in 1996 [1] and has become the favored fabrication tool for the production of holey fibers. The preform for MOF production is created by stacking several glass capillaries and rods to achieve the designed air-glass structure. Then MOF-preform is ready, the capillaries and glass rods are spliced together by thin wires and fused during an instantaneous drawing procedure. After that, the preform is placed onto a conventional fiber drawing tower, greatly extending its length, while reducing its cross-section, from a diameter of tens of
millimeters to hundreds of microns [36]. One can readily notice the versatility and simplicity of the “stack-and-draw” method that contributes to the development of various MOF designs, in particular, solid-core and hollow-core MOFs. Figure 2.7 illustrates this sequence of stack and draw.

![Figure 2.7: Schematic of the fabrication of microstructured optical fibers by the "stack-and-draw" method.](image)

### 2.6 Physical demonstrative approach to the waveguiding properties of hollow fibers

As an initial approximation to hollow-core fibers, we can consider the simplest model of an optical waveguide consisting of a hole in a dielectric (the schematic is illustrated in Figure 2.8) [37,38]. Thus, the Fresnel reflection at the interface created by the surface separating the air-filled core with the dielectric determines the optical losses of this waveguide (Figure 2.8) [38]. However, it is possible to substantially decrease the fiber losses of by increasing the reflection coefficient between the air-filled core and solid.
cladding interface e.g., by reflection from two media, using as a waveguide, a tube with a thin glass wall (tubular waveguide) and constructive interference of the light that is reflected from both surfaces of the capillary [38]. In this model the entire structure of the waveguide can be described within geometric optics in terms of a model of Fabry-Perot resonator, therefore, a band structure or the alteration of the resonances and antiresonances occur in the fiber transmission spectrum [38]. The reflection coefficient decreases when the light is perpendicular to the capillary wall (an incidence angle is almost $\pi/2$). As a result, that leads to high waveguiding losses. The reflection coefficient increases, when the resonance condition is violated (or the antiresonance condition is met), then the reflection coefficient from the capillary wall increases dramatically and the band structure in the transmission of optical fiber appears (Figure 2.8). Later, such a mechanism has been studied more extensively in [39] and the abbreviated name Antiresonant reflecting optical waveguide was introduced [38].

![Hollow waveguide and Tube waveguide](image)

*Figure 2-8: Cross- and longitudinal sections of the hollow (left) and tube (right) waveguides.*

2.7 Light guidance in hollow-core microstructured optical fibers

The employed soft-glass HC-MOFs have a considerably thick wall of the central capillary of ~1.8 μm (Figure 2.9).
Figure 2-9: The SEM images of the fiber end face and the capillary wall of the first cladding ring.

Due to comparatively large characteristic scales of the fiber microstructure, the mechanism of light guidance in the investigated HC-MOF can be described within geometric optics. In this regime, the spectral position of the fiber transmission windows is well described by the Fabry-Perot resonances and antiresonances in the wall of the central capillary so that the fiber transmission maxima (Eq. 2.12) and minima (Eq. 2.13) occur at [39,40]:

\[
\lambda_{j\,\text{max}} = \frac{4d}{2j+1} \sqrt{n_g^2 - n_e^2} \tag{2.12}
\]

\[
\lambda_{j\,\text{min}} = \frac{2d}{j} \sqrt{n_g^2 - n_e^2} \tag{2.13}
\]

where \( j \) is an integer describing the resonance/antiresonance order (\( j = 1, 2, 3, \ldots \)), \( n_e \) is the refractive index (RI) of the medium filling the capillaries, \( n_g \) is the RI of the fiber glass, and \( d \) indicates the wall thickness for the first capillary layer.

Thus, at wavelengths other than \( \lambda_{\text{min}} \), the light will be confined inside the air core with finite but low leakage loss [3]. In this spirit, the broadband and multiband light-g Guiding can be regarded as results of the slab shapes of the glass membranes [3]. Specifically, \( d = 1.8 \, \mu\text{m} \) and \( n_e = 1 \) results in 5 transmission windows in the visible and
near-infrared spectral domains (400 - 900 nm), and the transmission maxima appear at 437, 488, 553, 639 and 755 nm (for \( j = 9, 8, 7, 6, 5 \)). Figure 2.10 shows theoretical and experimental transmission spectra for an unmodified air-filled HC-MOF.

![Graph showing theoretical vs experimental transmission spectra for an unmodified and empty HC-MOF.](image)

*Figure 2-10: Theoretical vs experimental transmission for an unmodified and empty HC-MOF with a core diameter of 240 μm and the wall thickness for the first capillary layer of 1.8 μm [14].*

### 2.8 Functionalization of optical fibers

The recent development in thin films deposition technique enables the fiber surface modification with nano-coating layers and exploits the phenomena of surface plasmon resonance (SPR) [41,42], localized surface plasmon resonance (LSPR) [43,44] and lossy mode resonance (LMR) [45] for the surrounding medium change measurements through the shift of the plasmonic resonance position [46–48]. However, the strong influence of uniformity and thickness of the metal coating on sensing performance together with
complicated and high-cost thin-films deposition process makes these types of sensors not always optimal [43,49]. The necessity to cover the whole sensor surface prevents the work with low analyte volume that is crucial in bio-applications (Figure 2.11).

Figure 2-11: Optical fiber sensor based on SPR. Illustration of the working principle of the fiber-based SPR sensor. The shift of the plasmon resonant wavelength is associated with the change in the refractive index of the sample (dn) defining the resonant condition [48]

Among the different structures of OFSs and related microstructures [50], the sensors based on geometry-modified fibers (D-shaped, polished, etched and tapered) [46,51–53], grating-assisted fibers [54] and MOF [55,56] represent three the most developed OFS groups (Figure 2.12).
Figure 2-12: An overview of different structure modified optical fibers. (I) Geometry-modified optical fibers: (a) unclad, etched, (b) side-polished, D-shaped fibers, (c) hetero-core structures, (d) U-shaped fibers and (e) arrayed fiber end face. (II) Grating-assisted fibers. (III) Specialty fibers [46].

Nevertheless, the major challenge of the first two sensor structures is the low sensitivity for detecting small biomolecules and low analyte concentration. At the same time, such surface modifications as cladding removing, side polishing and fiber tapering leading to the enhanced detection sensitivity suffer from poor mechanical stability and complicated fabrication processes [11,49].

Recently, HC-MOFs or holey fibers, which structure is defined by an array of air-channels, running through the whole fiber length, have been extensively studied, using their unique characteristics to create highly sensitive chemical and biological sensors with an application in different fields of biophotonics, chemistry, and life science.
To date, the major efforts in the functionalization of hollow-core microstructured optical fibers (HC-MOFs) have been aimed at using three techniques: high pressure chemical vapor deposition, direct fiber drawing and layer-by-layer (LbL) assembly [9]. The first two methods are used to form coatings of plasmonic nanoparticles for Raman-microscopy-assisted and optofluidic refractive index sensing [20,57,58] while the LbL assembly allows coatings made of different functional nanoparticles and polymer nanofilms for in-fiber multispectral optical sensing [14] and label-free detection of target analytes [59].

MOF biosensitivity is achieved through the selective adsorption of target molecules onto fiber surfaces, that have been functionalized with antibodies in order to bind to specific antigens which are investigated [14,49–53]. Specific adsorption-based sensors are used for human disease diagnosis and prevention with a sensitivity that meets clinical needs [23,54] (Figure 2.13).

*Figure 2-13: The illustration of the concept of label-free optical biosensor [60].*

Dinish U.S. et al. reported a novel MOF-based surface-enhanced Raman scattering (SERS) sensor for the detection of cancer proteins in the very low sample volume [61] with a potential of the multiplex detection of biomarkers immobilized inside the hollow core
MOFs [62]. Ultrasensitive measurement of protein was achieved using anti-epidermal growth factor receptors (anti-EGFR) antibody conjugated SERS nanotag (Figure 2.14) and the simultaneous detection of hepatocellular carcinoma biomarkers-alpha fetoprotein and alpha-1-antitrypsin secreted in the supernatant from Hep3b cancer cell line was demonstrated [62]. It has been shown that the proposed detection method was sensitive to the low amount of proteins at $\sim 100$ pg in a sample volume of $\sim 10$ nL.

![Figure 2-14: The sketch of the functionalized fiber surface showing the binding of anti-EGFR antibody conjugated SERS nanotag to the cancer protein (positive human epithelial carcinoma cells A431) immobilized on the inner wall of the core of MOF [61].](image)

The biological sensors based on modified MOFs have found their applications for the selective detection of DNA. The functionalization of the fiber surface leads to the binding of biological species to the glass surface that is then proved through the measurement of the fluorescence signal created by the labeled sample [63].

Several groups reported the feasibility of MOF-based biosensors for DNA detection [64,65]. Ngyuen L.V. et al. proposed that functionalized MOFs can act as a highly specific
DNA sensor and experimentally demonstrated the detection of DNA in nanoliter-scale sample volumes [66]. The modification of the fiber surface consisted of a combination of the fuzzy nano assembly technique named also layer-by-layer assembly method [67] and the biotin-streptavidin binding mechanism. The authors showed that the created sensor allows for the detection of DNA solutions at a concentration of 4 µM with the potential for further improvement.

The major advantage of using hollow-core MOFs rather than other techniques based on geometry-modified optical fibers, cuvettes, and bulk optics, lies in combining the long interaction lengths with strong overlapping between the light mode, that penetrates deeply into the air capillaries via its evanescent field, and the injected analyte [16]. More practical approaches of using the accessibility of the air capillaries for the functionalization of the MOF surface were shown by Sukhishvili S. et al. on the example of solid and hollow-core MOFs [68]. Basically, the proposed methods combine both the advantages of microfluidics and fiber optics in a single MOF sample allowing light guidance with simultaneous liquid flow inside the hollow capillaries. The authors showed the fine accumulative SERS signal from the full-length Ag-nanoparticle functionalized MOFs as well as the potential for fine control of the density of deposited Ag nanoparticles and studied the SERS gain and light attenuation in the Raman intensity with MOF samples of different lengths [69].

The possibility of integrating colloidal bimetallic nanoparticles with predefined parameters into HC-MOFs was demonstrated by Ponce S. et al. [66]. With the proposed method, PtNi clusters became strongly attached to the inner surface of the hollow-core and
could be used as active catalysts for the hydrogenation of an azobenzene dye, opening new perspectives for \textit{in situ} catalysts monitoring.

An overview of the existing functionalization techniques and applied materials [70], their comparison, and the application areas can be found in References [11,71–75] and Table 2.1 summarizes the reviewed techniques applied for MOFs functionalization, their potential applications and describes the used MOF types.

\textit{Table 2-1: Summary of the MOF functionalization techniques and their potential applications} [10].

<table>
<thead>
<tr>
<th>MOF type</th>
<th>Functionalization</th>
<th>Application</th>
<th>Ref.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Suspended core</td>
<td>Selective deposition of different plasmonic nanoparticles into different hollow channels surrounding the central solid core</td>
<td>Simultaneous detection of two different biomolecules</td>
<td>[76]</td>
</tr>
<tr>
<td>Hollow-core</td>
<td>Selective filling of core and cladding air channels</td>
<td>Control of the number of guided modes; Single-mode guidance</td>
<td>[77,78]</td>
</tr>
<tr>
<td>Hollow-core and suspended core</td>
<td>Functionalization of fiber surfaces with antibodies specific binding to antigens under test</td>
<td>Specific adsorption-based sensors for human disease diagnosis and prevention; Selective adsorption of the target molecules onto fiber surfaces; MOF-based SERS sensor</td>
<td>[61,62]</td>
</tr>
<tr>
<td>Suspended core</td>
<td>Combination of the fuzzy nano assembly technique and the biotin-streptavidin binding mechanism; hybridization of immobilized peptide nucleic acid probes</td>
<td>Biosensor for selective DNA detection based on suspended-core MOF</td>
<td>[63–66]</td>
</tr>
<tr>
<td>Hollow-core</td>
<td>Silanization of the fiber inner walls</td>
<td>Creation of bio sensitive structure on the example of the covalent binding of horseradish peroxidase to the obtained silanol-modified fiber surface</td>
<td>[79]</td>
</tr>
<tr>
<td>Solid core and hollow-core</td>
<td>Finely tuned plasmonic layers of Ag-nanoparticles inside the air capillaries of MOFs; a combination of microfluidics and self-assembled monolayer method, leading to a uniform deposition of silver nanoparticles</td>
<td>Fine accumulative SERS signal from the full-length Ag-nanoparticle functionalized MOFs and fine control of the density of deposited Ag nanoparticles</td>
<td>[69,80–82]</td>
</tr>
<tr>
<td>Hollow-core</td>
<td>Integration of colloidal bimetallic nanoparticles with predefined parameters into HC-MOFs</td>
<td>In situ catalyst monitoring</td>
<td>[83]</td>
</tr>
<tr>
<td>Core Type</td>
<td>Description</td>
<td>Application</td>
<td></td>
</tr>
<tr>
<td>------------------------------</td>
<td>-----------------------------------------------------------------------------</td>
<td>------------------------------------------------------------------------------</td>
<td></td>
</tr>
<tr>
<td>Suspended core</td>
<td>Gold nanoparticles-functionalized suspended core MOF</td>
<td>Efficient RI sensing featuring the real-time analyte monitoring [13,84]</td>
<td></td>
</tr>
<tr>
<td>Suspended core and exposed core</td>
<td>Functionalization of hollow channels with a monoazacrown bearing spiropyran; attachment of the fluorophore to a polyelectrolyte-coated fiber’s surface</td>
<td>Biosensors for the reversible and low volume scale measurement of metal ions; real-time detection of zinc, aluminum and lithium ions [85–87]</td>
<td></td>
</tr>
<tr>
<td>Solid core</td>
<td>Integrated micron-sized Ge wire inside the air channel of modified step-index MOF</td>
<td>In-fiber detector and sensor [88]</td>
<td></td>
</tr>
<tr>
<td>Solid core and hollow-core</td>
<td>Silver metaphosphate/silica step-index fiber and an arsenic trisulphide waveguide embedded in silica produced by pressure-assisted melt filling</td>
<td>Supercontinuum generation [89,90]</td>
<td></td>
</tr>
<tr>
<td>Hollow-core</td>
<td>Doping glass materials with Thulium (Tm) and Erbium (Yb)</td>
<td>Generation of high power CW-lasing and the amplification of nanosecond pulses [91–93]</td>
<td></td>
</tr>
<tr>
<td>Hollow-core</td>
<td>LbL assembly of inversely charged polyelectrolytes and magnetite or silica particles at different diameters</td>
<td>Magnetic resonance imaging of hollow-core MOF; increased effective sensing area and the provision of a convenient scaffold for the binding of specific molecules [40,94]</td>
<td></td>
</tr>
<tr>
<td>Suspended core and hollow-core</td>
<td>Coating with quantum dots on the inner surfaces of hollow channels</td>
<td>CdSe/ZnS nanocrystals; detection of nitric oxide by using an exposed core MOF coated with CdTe/CdS core/shell quantum dots [95–97]</td>
<td></td>
</tr>
</tbody>
</table>

### 2.7 Polyelectrolytes

Polyelectrolytes are macromolecules that, when dissolved in a polar solvent like water, have a (large) number of charged groups covalently linked to them, and equivalent numbers of counter ions released to the solvent during the dissolution process [98]. Depends on the sign of charged groups positive or negative the polyelectrolytes can be divided into two types polycations and polyanions, respectively. These groups dissociate in aqueous solutions (water), making the polymers charged and release the counter ions into the solvent. Therefore, the properties of polyelectrolytes are similar to both electrolytes...
and polymers. The salts, i.e. the products of a polyacids (polyanions) with a monomeric base and vice versa are called polsalts. Like regular salts, their solutions are electrically conductive and like polymers, their viscosity strongly depends on the molecular weight and polymer concentration. The combination of polymeric and electrolyte behavior gives them many useful properties but also poses problems of characterization [99]. There are strong and weak polyelectrolytes. Strong polyelectrolytes are charged over a wide pH range [100]. Hence, it is a difficult task to manipulate the properties of the assembled film unless one takes specific measures to disturb the polymer-polymer interactions by controlling other stimuli such as ionic strength, temperature, and polarity. Unlike strong polyelectrolytes, weak polyelectrolytes are charged only in a smaller pH window; hence, their polymeric conformations can be easily modulated upon changing the pH of the external environment. The unique feature of polyelectrolyte multilayers (PEMs) films assembled from weak polyelectrolytes is that they can be destroyed at extreme pH conditions as the pH-induced charge imbalances in the film overcompensate the attractive polymer-polymer interactions [100,101].

Hong and Decher first proved the concept, i.e. the alternating exposure of a charged planar substrate to solutions of positive (cationic) and negative (anionic) polyelectrolytes [67,102,103]. Provided that each adsorption step leads to charge inversion of the surface, the subsequent deposition finally results in a layered complex, stabilized by strong electrostatic forces, so-called self-assembled PEMs [103].
2.8 Layer-by-layer assembly

The layer-by-layer deposition method is a powerful and reliable technique used to modify nanostructured materials and surfaces by various functional nanoparticles and multilayers [67,104]. In contrast to other fabrication tools, the LbL assembly offers excellent control and versatility and allows surface functionalization without the need for bulky and expensive laboratory equipment and complicated protocols [105,106]. The sequential deposition of self-assembled multilayers and the adsorption of target nanoparticles ensures the creation of advanced coatings with multiple functionalities in a highly controllable and reproducible way. Nano-scale accuracy of the produced structures over film thickness relies on the number of sequentially deposited cycles and can be tailored [107] by several assembly conditions such as surface charge [108], concentration, ionic strength [109] and pH level [110,111] of the applied solutions.

Figure 2-15: Schematic of layer-by-layer assembly of inversely charged polyelectrolytes onto the planar substrate. The immersion with water solution in between the deposition cycles ensures the elimination of unbounded particles. The deposition cycles are repeated until the desired number of layers is achieved.
Originally, self-assembled multilayers were developed to modify planar substrates by oppositely charged polyelectrolytes (Figure 2.15) [67], and later on, this approach was successfully implemented for the production of various particulate composite structures based on hybrid organic–inorganic multilayers including advanced core-shell models of submicron and nanoparticles [112,113]. Nowadays, LbL engineered structures with a wide range of properties have found their applications in many different fields, ranging from “smart” materials for optics and biotechnology [114] to drug delivery and medicine [113,115,116] and the potential to which this technique can be developed still motivates further research [104,106,117]. Such rapid development has been driven by an extensive choice of available materials and advanced assembly techniques, as well as the utilization of modern film characterization tools [106].

2.9 Stimuli-responsive layer-by-layer complexes

Although these LbL assembled multilayers are often uniform at the first blush, microscopic scale roughness is usually observed on a closer look [118]. For a deposition with a constant thickness increment, the surface roughness increases with the overall number of layers [14,118]. Thus, after substantial height variation, the rough coating appears extra light scattering due to surface topologies on the order of the wavelength of light that results in additional waveguiding losses that are unwanted in some applications based on optical properties of functional coatings [118].

To this extend, postmodification of multilayer films may result in the appearance of novel structures or advantageous structural changes in the film. The surface morphology of polymer layers is usually controlled through postprocessing by “annealing” in aqueous
solutions of different salt concentrations or pH levels. By controlling pH and ionic strength, it is possible to vary the thickness of adsorbed layers from ~1 to ~10 nm or, in some cases, completely prevent the multilayer deposition process [107,119]. Several research groups showed that treatment of polyelectrolyte multilayers in salt solutions caused swelling and led to smoother surfaces showing faster annealing for higher salt concentrations[118,120]. Treatment of multilayers with solutions at varying pH-induced morphological irreversible and reversible changes in both weak polyelectrolytes [101,119] and in H-bonded multilayers [121,122]. The intrinsic property of multilayers composed of weak polyelectrolyte complexes is that they can be destroyed at extreme pH conditions, as the pH-induced imbalance of charges overcompensates the attractive polymer-polymer ionic binding[123].

2.10 1D photonic crystal based sensing

Plasmonic biosensors realized on the platform of one dimensional (1D) photonic crystals demonstrate outstanding performance and sensitivity to detect alteration of the environment refractive index that rank them among the best candidates for different applications [124]. The operating principle of the surface plasmon resonance (SPR) sensor is based on the registration of the resonance associated with the excitation of surface plasmon-polaritons which are electromagnetic waves propagating along the metal-dielectric interface [124]. The spectral and angular positions of this resonance depend strongly on the optical properties of the surrounding medium.

The typical configuration of an SPR sensor is based on the Kretschmann or Otto architecture, both depicted in Figure 2.16. The high refractive index prism is used to match
the wavevector of the evanescent wave to the surface plasmon polariton at the interface between the conductor and analyte. In the Kretschmann configuration, the conductor is deposited as a thin film on the prism and the analyte is placed on the top. In the Otto configuration, the conductive material is pressed towards the prism, with the dielectric-analyte sandwiched between them [125]. In both the cases, SPR optical technique measures the refractive index changes in the vicinity of thin metal layers (i.e., gold, silver, or other plasmonic films) in response to the surrounding medium.

![Diagram](image)

**Figure 2-16:** In the Otto configuration uses a bulk plasmonic material is separated from the prism by a thin layer of a dielectric analyte. In the Kretschmann configuration, the plasmonic material is deposited as a thin film on the prism, with the dielectric analyte on top. In both cases, the prism is used to match the wavevector of the incident light to the wavevector of the surface plasmon polariton at the interface between the dielectric analyte and plasmonic material. Adapted from [125].

### 2.11 Capillary condensation phenomena

Water adsorption technologies have attracted a tremendous amount of interest due to their extensive applications in various research fields [126]. Condensation is the process where water vapor or gas substances become liquid. It is a reversible process to evaporation, where liquid water becomes a vapor. Gases can condense according to three different mechanisms: in the air (homogeneous nucleation), on the surface (heterogeneous
nucleation) and inside the pores. However, gas condensation in the pores occurs at the lowest partial gas pressures [127]. The pore diameter, where capillary condensation takes place, can be calculated via Kelvin equation (Eq. 2.14):

\[
\ln \frac{p}{p_0} = -\frac{2\sigma V_l}{\gamma_m R T},
\]

(2.14)

where \( p \) is the vapor partial pressure, \( p_0 \) is the saturated vapor pressure, \( \sigma \) is the surface tension, \( V_l \) is the molar volume of the liquid, \( R \) is the universal gas constant (8.314 J mol\(^{-1}\) K\(^{-1}\)), \( \gamma_m \) is the Kelvin radius of the mesopores, and \( T \) is Kelvin's temperature.

As mentioned above, the condensation process depends on the pore size, which in turn depends on the size of the individual particle forming the porous layer. For example, for a pore of 3 nm, the size of the spheres forming such a pore should be 25 - 30 nm. And for a micropore size of 17 nm, the diameter of the spheres should be 150 - 180 nm.

### 2.12 Opal-like photonic crystals

Photonic crystals are highly ordered structures that influence the propagation of light by their periodic variation in dielectric contrast or refractive index with periods on the scale of visible light wavelengths [128]. Photonic crystals exist throughout the natural world from opal gemstones and beetles to bird feathers and butterfly wings and the common characteristic between all is their iridescent color [128]. Traditionally, researchers have used two methods to fabricate photonic crystals: nanolithography and self-assembly of colloidal crystals [129]. The self-assembly of colloidal crystals is the more preferred way as it is a simple and inexpensive technique. This can yield crystalline samples of a few to several hundred structural layers thickness. The approach involves the crystallization of a colloidal dispersion of monodisperse spheres of silica, polystyrene or polymethylmethacrylate to form a material with a three-dimensional periodic structure in
which 24% of the volume is air (a colloidal crystal or opal). Photonic crystals exist throughout the natural world from opal gemstones and beetles to bird feathers and butterfly wings and the common characteristic between all is their iridescent color [130].

Figure 2-17: Schematic outlining the interaction of light with the periodic material (opal-like photonic crystal) with an effective refractive index, and the light scattered by the sphere planes. \( \theta_1 \) and \( \theta_2 \) are the angles between the normal to the sample surface and the direction of the incident and refracted light beams, respectively; \( n_{\text{eff}} \) and \( n_1 \) is the effective refractive index of the photonic crystal and the external medium, respectively. Adapted from [128].

A modification to Snell's law for refraction of light between media of dissimilar refractive index, and Bragg's law for optical diffraction can be derived to describe the wavelength-dependent ‘structural color’ observable in colloidal opals or opal-like photonic crystals. As outlined in Figure 2.17, the opal film is formed as a multilayer of two media with different refractive indices (\( n_1 \) is typically denoted to vacuum, air or a liquid, and \( n_{\text{eff}} \) that of the photonic crystal. In the case of constructive interference of diffracted photons, Bragg's law can be written as (Eq. 2.15) [128]:

\[
\sin \theta_1 = \sin \theta_2 = \frac{n_1}{n_{\text{eff}}}
\]
where $m$ is the resonance order, $d$ is the interplanar spacing defining the centroids of the spheres.

The effective refractive index, $n_{\text{eff}}$, of the photonic crystal depends on (Eq. 2.16) the refractive index of the embedded particles ($n_{\text{particles}}$), the refractive index of surrounding media, $n_{\text{medium}}$, ($n_{\text{air}} = 1$) and the packing density, $f$, (for an ideal close-packed structure of spheres $f = 0.7405$) [131]:

$$n_{\text{eff}} = \sqrt{n_{\text{particles}}^2 f + n_{\text{medium}}^2 (1 - f)}$$  \hspace{1cm} (2.16)

The corresponding Snell's law criterion for the light incident at an angle $\theta_1$ can be expressed as (Eq. 2.17):

$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$  \hspace{1cm} (2.17)

Thus, the angle-dependent diffraction or color can be written in terms of the incident angle generally as the Bragg–Snell law which takes into account refraction of light in the composite structure and the incident angle of the incoming light [128,130]:

$$m \lambda_m = 2d \sqrt{n_{\text{eff}}^2 - \sin^2 \theta_1},$$  \hspace{1cm} (2.18)

3. **Chapter 3. Functionalized optical fibers**

Experimental and theoretical results obtained in the scope of this Ph.D. thesis are presented in three separate chapters. Chapter 3 covers the surface functionalization of HC-MOFs and the material and optical characterization of the produced structures, including an overview of the different environmental conditions while LbL assembly with their specific advantages and disadvantages. Loss analysis of functionalized HC-MOFs concludes the fabrication chapter. Chapter 4 introduces silica particles functionalized photonic crystal-based sensors. Chapter 5 is devoted to different post-processing techniques directing to the smoothing of the original films and the creation of
biocompatible and removable nanocoating. In chapter 6, refractometric measurements based on the set of functionalized are presented on the example of bovine serum albumin (BSA) at different concentrations.

3.1 Introduction

To date, the major efforts in the functionalization of HC-MOFs have been aimed at using three techniques: high-pressure chemical vapor deposition, direct fiber drawing and LbL assembly. The first two methods are used to form coatings of plasmonic nanoparticles for Raman-microscopy-assisted and optofluidic refractive index sensing [9,20,57,58] while the LbL assembly [67] allows coatings made of different functional nanoparticles and polymer nanofilms for in-fiber multispectral optical sensing [14] and label-free detection of target analytes [59]. Despite the challenges of coating fabrication on a non-conventional substrate formed by curved fiber surfaces, LbL assembled multilayers were successfully applied for the functionalization of different kinds of OFs [132] with the materials which were traditionally not used in fiber optics [10]. Depending on the coating function, that can be either buffer layers with a predefined value of surface potential [108] for selective capture of target particles and better adsorption of specific molecules and functional nanoparticles [59,61,62] or the complete bioresponsive layers [133] with predefined released characteristics.

Diverse fiber structures give a rise to various deposition approaches, differing by the location of host materials integration. Functional films can be deposited onto both the outer surface [133] and the inner regions of hollow capillaries of MOFs as well as onto the fiber tip. In both cases, the produced films became a key feature of functionalized OFs
since they control and dictate interactions of the guided light with the surrounding environment that defines the optical properties of modified OFs [106].

Among the variety of produced structures, HC-MOFs, which consist of air channels running along their whole length, represent an attractive playground for the creation of multifunctional in-fiber optical sensors [14]. The major advantage of application HC-MOFs lies in combining the long interaction length with strong overlapping between light and the analyte within small sample volumes, giving rise to high sensitivity [11]. Thus, any variations in the composition of the fiber surface and/or the filled media can be detected by measuring the shifts of maxima and minima in the transmission spectrum of HC-MOF [11]. The feasibility of the LbL assembly technique for an accurate coating of fiber capillaries with polymer nanofilms consisted of polyelectrolyte multilayers and the creation of HC-MOF-based multispectral optical sensor was recently demonstrated [14]. Furthermore, the experimental conditions can be adopted to load submicron silica particles into the central hollow-core of MOFs which were initially modified with polyelectrolyte multilayers [94] serving as a substrate for particle adsorption. However, LbL functionalization of the inner surface of the light-guiding hollow-core induces additional fiber losses. This remains negligible for thin films and does not significantly disturb light guidance inside the fiber as long as the number of bilayers is limited [14]. Nevertheless, extra light scattering due to surface features on the order of the wavelength of light decreases the sensitivity at single or multiple wavelengths followed by a spectral broadening of any type of optical resonances [94].
3.2 Motivation

Spectral properties of HC-MOFs are defined in the fabrication step and are mainly depend on the refractive index of glass material and the thickness of the first cladding ring. Thus, due to the limited number of accessible materials satisfying the fiber optics needs, variation of the capillary thickness has been found as the only way to control the optical properties of HC-MOFs. However, reproducibly drawing fiber families with slightly different thicknesses of the first cladding ring ($\Delta \sim 10$ nm) is technically quite a challenging task that would inevitably increase the cost of fiber production. Therefore, the postprocessing technique that could tune in a reproducible and highly controllable way the transmission windows in both visible and IR-spectral range through the modification of the fiber surface is highly disabled. In the next section, this issue has been resolved by presenting a simple and inexpensive technique applied for surface functionalization. This allows a small increase in the thickness of capillary walls leading to the appearance of several MOFs with slightly shifted transmission windows that were originally drawn from the same preform [14].

However, any modification of the internal structure of fiber capillaries changes the conditions for the light guidance since any imperfections (defects) and height variations featured rough surfaces give a rise to extra scattering losses. Therefore, the analysis of transmission losses in the functionalized fibers is required to study the effect of modification on light propagation. All the previously published works disregard this evaluation which is crucial for understanding the limitations of functionalization from the point when it has a negligible effect to the case of complete disturbance of light guidance.
Here, a detailed study of the light propagation in functionalized fibers with polymer nanocoating at different thicknesses has been performed.

Besides, all the previous works on this topic have demonstrated sensing functionalities of MOFs for capillaries with smooth walls [10,11]. In this contribution, the technique for HC-MOFs coating with chemically and mechanically stable, monodisperse submicron silica particles by the layer-by-layer deposition approach has been developed. The proposed method of MOF functionalization allows one to reach novel sensing capabilities, including an increase in the effective sensing area, providing a convenient scaffold for the attachment of long molecules such as proteins, and combining in-fiber liquid sensing and high-performance liquid chromatography [134]. The surfaces, which are covered with closely packed spherical particles, can also serve as promising sensitive elements of gas sensors [135] due to capillary condensation in the gap formed with particles in contact.

3.3 Materials and methods

3.3.1 HC-MOF samples

The reported HC-MOFs were produced by a stack-and-draw method described in [136]. Three concentric capillary layers surround the central hollow-core and define the overall fiber structure. The geometrical features of the HC-MOF are detailed in Figure 3.1.
Figure 3-1: SEM images of the HC-MOF used in the experiments. (a) General view. (b) Inset showing the wall thickness of the central capillary.

The wall thickness of the capillaries forming the first cladding layer was ~1.8 μm, the diameter of the hollow-core was ~240 μm, and the outer diameter was ~600 μm. Such a fiber structure supports multimode guidance. Spectral properties of HC-MOFs have been discussed in detail in [4,137].

The optical dispersion of glass material is illustrated in Figure 3.2.
3.3.2 Chemical reagents

All applied PEs were purchased from Sigma-Aldrich: poly (allylamine hydrochloride) (PAH) (MW = 50,000), poly (styrene sulfonate) (PSS) (MW = 70,000), poly (diallyldimethylammonium chloride) (PDDA) (MW = 400,000 – 500,000) and polyethylenimine (PEI) (MW = 2,000,000). Chemical structures of the applied polyelectrolytes are illustrated in Figure 3.3.

![Chemical structures of the polyelectrolytes](image)

**Figure 3-3:** Chemical structure of the polyelectrolytes used for the creation of functional coatings (PAH - poly (allylamine hydrochloride), PSS - poly (styrene sulfonate), PDDA - poly (diallyldimethylammonium chloride) and PEI - polyethylenimine).
Magnetic nanoparticles (MNPs) were prepared by chemical precipitation from a solution of FeCl$_3$ and FeCl$_2$ salts under sodium hydroxide [138]. Super monodispersed silica nanoparticles were prepared by using the multistep method described in Reference [139]. Deionized water was produced by a Millipore Milli-Q Plus 185 system.

3.3.3 Multilayered deposition process

The basic principle of our approach is the LbL assembly of oppositely charged PEs onto the glass surface. Figure 3.4 shows the setup used for coating the fiber capillaries [94].

![Image of setup for functionalization of HC-MOFs with LbL assembly](image)

*Figure 3-4: The setup for functionalization of HC-MOFs with LbL assembly. A peristaltic pump drives the flow of applied solutions (polyelectrolyte water solution, silica particles colloid solution, magnetite particles colloid solution and pure water) through the full fiber length, leading to the formation of the polymer coating on the inner surface of the core capillary. The procedure is repeated to create the desired number of bilayers. The insets depict the scanning electron microscopy (SEM) images of the fiber end face. Adapted from [14].*

The peristaltic pump creates a flow of PE solutions through the fiber with a controllable and persistent rate for a pre-determined volume. This procedure results in the uniform deposition of PE layers inside the fiber capillaries. As polyelectrolytes, aqueous solutions of polycationic PAH, PEI or PDDA and polyanionic PSS [140] have been used.
As functional materials, silica submicron particles at different diameters and magnetite nanoparticles were incorporated into polymer substrate formed by PE multilayers [94,141].

Prior to PE layer assembly, the fibers were washed with deionized water for 2 min with a speed of 500 μL min\(^{-1}\) to ensure that small dust particles were removed; then, the fibers were subjected to the LBL technique by a combination of inversely charged PEs and/or functional particles. The very first deposited PE layer consists of polyethylenimine (PEI) serving as an adhesive or anchor agent that provides a high surface charge density with a homogenous distribution due to its high molecular weight and branched structure [142,143]. Then, three material combinations were used to finalize the LbL assembled nanocoating. First is the combination of inversely charged PE solutions consisted of PAH and PSS which were prepared in water buffer and in the presence of 0.15 M NaCl. The second combination includes the positively charged PDDA polyelectrolyte and negatively charged silica particles at different submicron diameters. As the third set of applied materials, polycationic PAH and polyanionic magnetite nanoparticles has been applied for the LbL assembly. Deionized water was applied after each deposited layer of functional materials with a speed of 200 μL min\(^{-1}\) for 2 min to wash the samples and to remove unadsorbed molecules.

### 3.3.4 Optical transmission of functionalized MOFs

Optical measurements of MOFs samples were performed by the transmission setup based on CCD-spectrometer Ocean Optics QE Pro operating in the extended wavelength range and a broadband light source - Thorlabs SLS201L halogen lamp. The incoming light was launched into a MOF sample by the 10X Olympus objective and the output signal was
collected by the 10X Olympus objective and then send to spectrometer for spectral analysis (Figure 3.5).

![Schematics of the transmission measurement setup. 10X states for the 10X Olympus objectives.](image)

For the near-IR spectral domain, Ocean Optics QE Pro spectrometer has been replaced by a NIR spectrometer with 900 – 1700 nm wavelength range (NIRQuest, Ocean Optics, USA). In this case, silica-based auxiliary fiber cables (Art photonics GmbH, Germany) with 200/220 µm core/cladding diameters and 600/660 µm were utilized for the delivery of lamp illumination and the collection of light transmitted through MOF samples, respectively. To ensure the effective face-to-face connection between auxiliary fibers and MOF samples, the waveguide end faces were sealed into special SMA terminators and mounted into SMA/SMA connection sleeves, enabling their optical alignment. Measurements in the mid-IR spectral range were conducted with a Fourier-transform infrared (FTIR) spectrometer, operating in the broad spectral domain from 1.45 to 20 µm (Matrix-F, Bruker, Germany). Chalcogenide IR-fibers 180/280 µm and polycrystalline IR-fibers 240/300 µm (both supplied by Art photonics GmbH, Germany) were used for the light delivery in the ranges 1.1 - 6.5 µm and 3 - 18 µm, respectively. Chalcogenide 500/550 µm and polycrystalline IR-fibers 900/1000 µm (both supplied by Art photonics GmbH, Germany) ensured the effective light collection.

### 3.4 Results and discussion

In this section, the designed coatings are characterized from both material and optical points of view. Scanning electron microscopy (SEM) images of the fiber cross-sections help to evaluate the morphology of produced structures; average thickness and roughness are extracted based on the analysis of different fiber parts. Transmission spectra
measurements of functionalized fibers allow tracking the shift of the transmission windows during the multicycle coating formation. The cut-back method is performed for the analysis of the waveguiding losses induced by deposited layers.

3.4.1 Morphology of PAH-PSS multilayers

It has been shown for the planar substrates that the thickness of LbL assembled coatings is linearly proportional to the number of deposited layers [144,145]. Moreover, the thickness of LbL-assembled layers on a planar substrate is proportional to the square root of the ionic strength that, in turn, is the square function of the molar concentration of ions [146]. Hence, the ionic strength is typically supported by sodium and chlorine ions. For example, the thickness per single layer is 1.3 ± 0.1 nm at 0.05 M NaCl but is 2.2 ± 0.1 nm at 0.5 M NaCl [146]. In addition, the higher concentration of sodium chloride gives rise to an increased roughness caused by altering the molecular conformation from a linear to globular structure [14].

To gain insight into the impact of the solution ionic strength on the coating performance, thickness and morphology of assembled PAH/PSS films with PEs at the same concentration dissolved in deionized water and in buffer containing 0.15 M NaCl were studied systematically. Figure 3.6 shows the thickness of the coatings prepared by the alternating deposition of PAH and PSS layers from PE solutions with and without NaCl as a function of the number of deposited PE bilayers. The coating thickness linearly depends on the number of assembled PAH/PSS bilayers. However, the average thickness increase is 1.8 ± 0.3 nm and 7.0 ± 1.3 nm per bilayer for the salt-free PE solutions and in the presence of 0.15 M NaCl, respectively. These values differ from previously published data.
for LbL coating of planar substrates, where the average thickness per PE layer was ~1–3 nm [145,147,148]. This discrepancy is attributed to different hydrodynamic conditions for PE adsorption in our study and the effect of the charged capillary surface. An increase in the film thicknesses with increasing ionic strength in the PE solutions was also observed. This result is in good agreement with previously published works on the LbL coating of planar substrates.

![Graph showing polymer coating thickness versus the number of PE bilayers.](image)

*Figure 3-6: Polymer coating thickness versus the number of PE bilayers. The thickness is fitted to obtain the coincidence of the minima positions for both the experimental and calculated transmission spectra. Error bars show the coating roughness. Adapted from [14].*

The thickness of fiber coating can be evaluated via SEM micrographs (SEM) of the HC-MOF cross-section (as showed in Figure 3.6 above) and adjustment of the polymer coating thickness in the theoretical model (transmission) to get coincidence with the experimental transmission spectrum (Figure 3.7). Both approaches are in good agreement with each other.
Figure 3-7: Comparison of the experimental fiber transmission spectra with the theoretical ones obtained by adjusting the thickness of the polymer coating (60 nm per 40 polymer bilayers) [14].

3.4.2 The structure of silica particle-based fiber coating

LBL deposition is based on alternative adsorption of oppositely charged polyelectrolytes and silica particles. The very first layer includes three polyelectrolytes PEI/PSS/PDDA. Then four PSS/PDDA bilayers were applied to finalize the formation of the buffer layer aimed at strong adhesion for SiO$_2$ particles. SiO$_2$ particles with diameters of 300 nm, 420 nm and 900 nm have been utilized in the experiment [94].

Silica nanoparticles at the diameters of 300 nm and 420 nm homogeneously cover the almost full surface of the core capillary after the single layer is deposited (Figure 3.8).
Figure 3-8: SEM images of MOF end faces and magnified capillary surfaces. (a) MOF sample after deposition of one layer of 300-nm silica particles. (b) MOF sample after deposition of one layer of 420-nm silica particles [94].

In contrast to smaller particles of 300-nm and 420-nm, the bigger silica particles of 900-nm form layers on both sides of the first cladding ring (Figure 3.9).

Figure 3-9: SEM images of MOF end face (a) and magnified capillaries (b,c) with one deposited layer of 900-nm silica particles [94].

This can be explained by Stoke’s law. The viscosity force $F$ which describes particles flow inside the capillaries is proportional to their size and velocity (3.1):

$$F = 6\pi \mu R \nu,$$

where $\mu$ is the dynamic viscosity, $R$ is particle radius, $\nu$ is the flow velocity. (3.1)
The bigger silica particles are affected by the stronger viscosity force (Eq. 4), leading to slowing them down and, as a result, to a higher chance of their adsorption onto capillary walls. This is well-illustrated by the strong difference between the deposition of small (300-nm and 420-nm) and large (900-nm) silica particles. In the first case, particles adhere to the internal surface of the central capillary only; where is in the second case particles additionally adsorb to the first layer capillaries.

Next, MOF coating with three deposited layers of 300-nm silica nanoparticles has been analyzed (Figure 3.10). It should be noted that silica particle adsorption to a buffer polyelectrolyte layer is more efficient than deposition of the second and the third SiO$_2$ particle layers. The intermediate PDDA layer applied between silica particles serves as a recharger and is aimed at their better adsorption. However, due to its small thickness (in the range of 3 nm), a smaller number of silica particles are adsorbed.

![Figure 3-10](image)

*Figure 3-10: (a) SEM image of MOF end face; (b,c,d) magnified SEM images of capillaries with one, two and three deposited layers of 300-nm silica particles, respectively [94].*

To increase the concentration of adsorbed silica particles for multilayer deposition, the effect of intermediate polyelectrolyte layers has been studied and the two material
combinations have been compared: single PDDA layer and combination of PDDA/PSS/PDDA applied between SiO$_2$ particles. The triple polyelectrolyte layer was chosen to form the necessary thickness for better silica particle adsorption. The higher concentration of SiO$_2$ particles deposited on the core surface is shown in Figure 3.11.

![Figure 3-11: SEM image of MOF capillaries with two layers of 300-nm SiO$_2$ nanoparticles for the cases of (a) PDDA/PSS/PDDA and (b) PDDA intermediate layers, respectively at different magnifications top and bottom [94].](image)

SEM images of MOF hollow-core regions proved the concept of silica layer formation and showed the higher particle concentration for two deposited layers with a triple layer of PDDA/PSS/PDDA than the silica concentration with a single PDDA layer deposited.

### 3.4.3 Magnetite-based nanocoating for functionalization of microstructured optical fibers

A simple and cheap method of making HC-MOFs visible in magnetic resonance imaging (MRI) has been introduced in the example of fiber coated with magnetite-based nanoparticles which pave the way for combing MRI and optical bioimaging [40]. The proposed approach is based on the LbL assembly of oppositely charged polycationic polyelectrolytes and polyanionic magnetite nanoparticles (MNPs) on the inner core surface.
of HC-MFs. In this work, the formation of the composite nanocoating has been studied further for the increasing number of deposited bilayers. From SEM images of MOF cross-sections focusing on the inner surface of the hollow-core, one can observe the clear formation of the nanocoating resulted from the deposition of PEs and MNPs (Figure 3.12).

![SEM images of MOF cross-sections](image)

*Figure 3-12: (a) SEM image of MOF end face with the highlighted region of the inner surface of the hollow-core. (b,c) Magnified regions of the capillary walls illustrating the formation of composite nanocoating on the example of MOF samples modified with (b) 13 PAH/MNPs bilayers and (c) 28 PAH/MNPs bilayers [141].*

The average thickness of the coating formed by the deposition of 13 PAH/MNPs bilayers is equal to 85 nm and the one for the sample modified with 28 PAH/MNPs bilayer is 216 nm.

### 3.4.4 Optical characterization of MOFs functionalized by polymer multilayers

HC-MOF functionalization with an nm-thick polymer coating leads to fine-tuning of their optical transmission windows, as shown in Figures 3.13 and 3.14. Specifically, shifts in maxima and minima of the transmission appear to be almost a linear function of the number of deposited bilayers for both the buffer combinations (in salt-free PE solution and in the presence of 0.15M NaCl). This fact results from the similar RIs of the fiber glass [149,150] and PAH/PSS [151,152]; thus, polymer coatings can be considered an effective instrument to vary the thickness of the core fiber capillary.
Figure 3-13: Optical characterization of HC-MOFs functionalized by PEs adsorbed from the salt-free buffer (see Fabrication chapter). (a,b) Transmission spectra in the visible (400 nm – 900 nm) and near-infrared (900 nm – 1500 nm) ranges. The results for 6 samples with various numbers of PE bilayers are presented. Note the different scales along the x-axis for (a) and (b). Shifts of maxima (c) and minima (d) of the transmission along with the linear fits. Adapted from [14].
Figure 3-14: Optical characterization of HC-MOFs functionalized by PEs dissolved in saline buffer (0.15 M NaCl). (a) Transmission spectra in the visible range. The results for 6 samples with a different number of PE bilayers are presented. Shifts of maxima (b) and minima (c) of the transmission along with the linear fits [14].
Importantly, LbL functionalization results in additional transmission losses. The results of cut-back measurements for the samples modified in the salt-free PE solution are presented in Figure 3.15. One can observe that the polymer coating leads to an average extra attenuation of $\sim 0.02 \, \text{dB cm}^{-1}$ per single assembled PAH/PSS bilayer. However, this issue does not significantly disturb light guidance inside the fiber as long as the number of bilayers is limited.
Figure 3-15: Characterization of optical losses in functionalized HC-MOFs by the cut-back technique. (a) Unmodified MOF. Fibers coated with 14 (b) and 40 (c) PE bilayers in the salt-free solution. Shadow areas show the error range. (d) The minimal optical loss in the transmission windows as a function of the bilayer quantity. Adapted from [14].
3.4.5 Optical characterization of MOFs functionalized by silica particles

Figure 3.16 exhibits transmission spectra of MOFs coated with the buffer layer only and 300-nm and 420-nm silica nanoparticles. Deposition time and flow rate were equal for SiO₂ particles of both sizes. A layer of silica nanoparticles impacts on the position of optical resonances (Eqs. 2.12 and 2.13) similarly to the polymer layers, i.e. they induce the redshift of transmission spectra of functionalized MOFs. Experimentally measured spectral shifts obey this explanation and are in good agreement with the ones calculated from Equations 1 and 2 for the deposition of 300-nm and 420-nm silica particles and the effective thickness of applied layers of 106 nm and 125 nm, respectively (Table 3.1).

![Graph showing spectral shift of local transmission bands for MOF samples with one deposited layer of 300-nm and 420-nm SiO₂ particles into MOFs with an internal buffer layer.](image)

*Figure 3-16: Spectral shift of local transmission bands for MOF samples with one deposited layer of 300-nm and 420-nm SiO₂ particles into MOFs with an internal buffer layer [94].*
Table 3-1: Transmission peaks shift of MOF samples with one deposited layer of 300-nm and 420-nm SiO₂ particles [94].

<table>
<thead>
<tr>
<th>Peak number</th>
<th>Spectral shift measured, nm</th>
<th>Spectral shift calculated, nm</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>300-nm SiO₂</td>
<td>420-nm SiO₂</td>
</tr>
<tr>
<td>peak1</td>
<td>31 ± 2</td>
<td>38 ± 2</td>
</tr>
<tr>
<td>peak2</td>
<td>39 ± 2</td>
<td>45 ± 2</td>
</tr>
</tbody>
</table>

It is instructive to note that further growth of silica nanoparticle size leads to deterioration of the shape of the MOF transmission curve as a result of strong light scattering. For example, MOF coating by a suspension of 900-nm silica nanoparticles leads to significant deformation of the spectral curve (Figure 3.17).

Figure 3-17: Transmission spectrum of MOF sample with one deposited layer of 900-nm silica particles (blue). MOF spectrum with a buffer layer (red) [94].
Such double coating of silica particles on the first cladding ring (Figure 3.19) results in the disappearance of the Fabry-Perot anti-resonances, associated with local bands in the transmission spectra.

Next MOF coating with three layers of 300-nm silica nanoparticles has been analyzed (Figure 3.18). It should be noted that silica particle adsorption to a buffer polyelectrolyte layer is more efficient than deposition of the second and the third \( \text{SiO}_2 \) particle layers. The intermediate PDDA layer applied between silica particles serves as a recharger and is aimed at their better adsorption. However, due to its small thickness (in the range of 3 nm), a less number of silica particles are adsorbed. This effect is illustrated in Figure 3.18 where the highest spectral shift was measured for the first deposited silica particles layer (Table 3.2).

![Transmission spectra for MOFs coated with the buffer layer only (red) and with one (blue), two (black) and three (green) layers of 300-nm SiO\(_2\) particles](image-url)

*Figure 3-18: Transmission spectra for MOFs coated with the buffer layer only (red) and with one (blue), two (black) and three (green) layers of 300-nm SiO\(_2\) particles [94].*
Table 3-2: Spectral shift of local transmission bands for MOF samples with multiple deposited silica particle layers. The diameter of silica particles is 300-nm [94].

<table>
<thead>
<tr>
<th>Band number</th>
<th>1 layer</th>
<th>2 layers</th>
<th>3 layers</th>
</tr>
</thead>
<tbody>
<tr>
<td>peak1</td>
<td>31 ± 2</td>
<td>37 ± 2</td>
<td>42 ± 2</td>
</tr>
<tr>
<td>peak2</td>
<td>39 ± 2</td>
<td>42 ± 2</td>
<td>46 ± 2</td>
</tr>
</tbody>
</table>

3.4.6 Optical characterization of MOFs functionalized by composite multilayers

Optical transmission and fiber losses of HC-MOF samples functionalized by composite nanocoating formed by polyelectrolytes and magnetite nanoparticles have been also studied (Figure 3.19a). Thus, the set of MOF samples modified with a different number of PAH/MNPs bilayers was investigated on optical setup and the position of maxima located near 550 nm was tracked down (Figure 3.19b).

![Figure 3-19: (a) Comparison on transmission spectra of non-modified and modified MOFs. (b) The spectral shift of the maximum transmission spectrum located at 550 nm induced by the deposition of composite nano-coating on the inner surface of MOF hollow-core. The dashed line shows the linear fit of the experimental points. The error bars correspond to the spectrometer's optical resolution. Adapted from [141].](image)

The additional fiber losses induced by the formed composite nanocoating were estimated using the cut-back technique consisted of a series of three consistent cut-back steps performed on an initial 6 cm long MOF samples (Figure 3.20).
Figure 3-20: (a) Fiber loss of non-modified (empty) MOF sample. (b,c) The loss estimation of MOF samples modified with (b) 11 and (c) 23 PAH/ MNPs (Fe₂O₃).
Adapted from [141].

3.4.5 Demonstration of mid-IR guidance in designed HC-MOFs

To finalize optical characterization mid-IR guidance has been demonstrated. Figure 3.21 summarizes the results of transmission spectra measurements and loss analysis of investigated MOFs. The broadband guidance was observed from 400 nm to 14 µm (where signal-to-noise ratio was adequate) with clearly defined optical resonances in the mid-IR spectral domain and minimum loss of ~1 dB cm⁻¹ (2 - 4 µm transmission window). Minimal
losses in the near-IR region were observed in 0.8 - 1 µm transmission window and were equal to ~0.6 dB cm\(^{-1}\). Although the produced waveguides suffered from high material absorption beyond ~7 µm, clearly defined optical resonances in the wide wavelength range of 400 nm – 6.5 µm can open previously unreachable horizons for the soft glass-based MOFs applications.

Using the general transfer matrix method and taking into account the model of the Fabry-Perot resonator [40], the resonance positions of the investigated HC-MOFs have been calculated referring to the minima of transmission spectra.

\[\text{Figure 3-21: Demonstration of broadband VIS – mid-IR light guidance. Blue curve states for the transmission spectrum of investigated MOFs, the shaded region illustrates the estimated loss interval summarizing the results of 4 samples of MOFs. The red dotted line is the calculated spectrum referred to the positions of minima in MOFs transmission [8].}\]

A comparison of the designed borosilicate soft glass-based HC-MOFs and previously reported works is given in Table 3.3, emphasizing the microstructured and holly waveguides. HC and SC state for hollow- and solid-core, NC F means negative curvature fiber. Very few works report the effective fabrication and mid-IR guidance with HC-MOFs made from soft glasses. Russell et al. [153] achieved photonic bandgap guidance with soft-glass hollow-core PCF in the range of 750 – 1050 nm. Other groups concentrated on soft glass solid-core PCFs and achieved broadband transmittance up to 3 µm [154–156].
Dianov et al. succeeded in the production of silica negative curvature fibers and demonstrated mid-IR transmittance up to 7.9 µm [157]. Despite high material absorption in the IR spectral domain, few research groups received outstanding results in the fabrication of silica-based hollow-core fibers for mid-IR applications [158,159].

Table 3-3: Comparison of the optical performance of reported microstructured optical fibers [8].

<table>
<thead>
<tr>
<th>Waveguide type</th>
<th>Material</th>
<th>Guidance, nm</th>
<th>Loss</th>
<th>Authors</th>
<th>Year</th>
</tr>
</thead>
<tbody>
<tr>
<td>HC MOF</td>
<td>soft glass</td>
<td>400 – 6500</td>
<td>1 dB/cm</td>
<td>This work</td>
<td>2020</td>
</tr>
<tr>
<td>HC PCF</td>
<td>soft glass</td>
<td>750 – 1050</td>
<td>0.74 dB/m</td>
<td>Russell et al. [153]</td>
<td>2011</td>
</tr>
<tr>
<td>SC PCF</td>
<td>soft glass</td>
<td>900 – 2300</td>
<td>2 – 5 dB/m</td>
<td>Klimczak et al. [155]</td>
<td>2014</td>
</tr>
<tr>
<td>SC PCF</td>
<td>soft glass</td>
<td>350 – 3000</td>
<td>-</td>
<td>Russell et al. [154]</td>
<td>2006</td>
</tr>
<tr>
<td>SC PCF</td>
<td>soft glass</td>
<td>800 - 2600</td>
<td>-</td>
<td>Klimczak et al. [156]</td>
<td>2014</td>
</tr>
<tr>
<td>NC HC F</td>
<td>silica</td>
<td>2500 - 7900</td>
<td>50 dB/km</td>
<td>Dianov et al. [157]</td>
<td>2013</td>
</tr>
<tr>
<td>HC PCF</td>
<td>silica</td>
<td>2900 - 3250</td>
<td>2.6 dB/m</td>
<td>Knight et al. [160]</td>
<td>2005</td>
</tr>
<tr>
<td>NC HC MOF</td>
<td>silica</td>
<td>&gt;3500</td>
<td>1 – 10 dB/m</td>
<td>Dianov et al. [161]</td>
<td>2011</td>
</tr>
<tr>
<td>HC PCF</td>
<td>silica</td>
<td>1450 - 2100</td>
<td>6.5 dB/km</td>
<td>Zhang et al. [158]</td>
<td>2019</td>
</tr>
<tr>
<td>HC PCF</td>
<td>silica</td>
<td>1400 - 2300</td>
<td>9.5 dB/km</td>
<td>Roberts et al. [162]</td>
<td>2009</td>
</tr>
<tr>
<td>HC PCF</td>
<td>silica</td>
<td>3100 - 3700</td>
<td>0.05 – 0.13 dB/m</td>
<td>Richardson et al. [159]</td>
<td>2014</td>
</tr>
<tr>
<td>HC F</td>
<td>silica</td>
<td>3000 - 4000</td>
<td>34 dB/km</td>
<td>Knight et al. [163]</td>
<td>2012</td>
</tr>
<tr>
<td>3D HC MOF</td>
<td>polymer</td>
<td>3500 – 500</td>
<td>10 – 25 dB/mm</td>
<td>Talataisong et al. [164]</td>
<td>2018</td>
</tr>
<tr>
<td>Kagome HC F</td>
<td>silica</td>
<td>1000 - 3000</td>
<td>10 – 14 dB/km</td>
<td>Richardson et al. [165]</td>
<td>2017</td>
</tr>
<tr>
<td>SC PCF</td>
<td>ZBLAN</td>
<td>200 - 2500</td>
<td>-</td>
<td>Russell et al. [166]</td>
<td>2015</td>
</tr>
</tbody>
</table>

3.5 Summary

In this chapter, layer-by-layer assembly of polymers and/or inorganic nano- and submicron particles has been successfully adapted for the functionalization of the inner surface of HC-MOFs. A detailed explanation of the experimental techniques along with the necessary study of the coating performance versus the number of deposited bilayers confirmed the concept of high control and repeatability of produced structures. We have adapted the LbL technique to accurately coat fiber capillaries with polymer nanofilms. The effect of salt presence in the applied PE solutions on the coating performance has been considered. In contrast to the salt-enriched PEs, the salt-free PE solutions yield the smallest roughness and coating thickness per single bilayer. The average thickness increasing of 1.8 ± 0.3 nm and 7.0 ± 1.3 nm per PAH/PSS bilayer for the salt-free PE solutions and in the presence of 0.15 M NaCl, respectively, has been observed [14]. Thus, the polymer coating
leads to an average extra attenuation of ~0.02 dB cm\(^{-1}\) per single assembled PAH/PSS bilayer formed in salt-free PE solution [14]. The proposed LbL deposition technique can be extended further, allowing one to reach novel sensing capabilities including HC-MOF functionalization by specific molecules to capture biomolecules (DNA, antibodies, aptamers, Fab, etc.) and target particles.

For the first time to our knowledge, the LBL technique for HC-MOF modification through the deposition of silica particles with different sizes (300, 420, and 900 nm) onto capillary surfaces has been presented [94]. The potential for the creation of multilayer porous coating was demonstrated on the example of one, two, and three layers of 300-nm silica particles. The largest spectral shift in the transmission is induced by the first deposited silica layer (31 nm and 39 nm, for the first and the second transmission bands, respectively), while additional silica layers are worse-adsorbed on the first layer of particles, resulting in the additional transmission spectral shifts (11 nm and 7 nm). Additionally, the synergy of MRI and optical fiber-based endoscopic probe was presented in HC-MOFs functionalized with magnetite nanoparticles [141].

Additionally, the transmittance of investigated HC-MOFs was characterized in a broad spectral range. Effective light guidance in the spectral region of 400 nm - 6.5 µm with the minimum loss of ~0.6 dB cm\(^{-1}\) in the near-IR spectral domain (0.8 - 1 µm transmission window) and minimum loss ~1 dB cm\(^{-1}\) in the mid-IR region (2 - 4 µm transmission window) was observed [8].
4. Chapter 4. Silica particles functionalized photonic crystal based sensor

4.1 Motivation

In a commercial SPR biosensor configuration, incident light is employed by using a high-reflective index glass prism in the Kretschmann geometry (Figure 2.16b). The defined SPR angle, at which resonance occurs, is dependent on the refractive index of the material covered the metal surface. Consequently, when there is a small change in the refractive index of the sensing medium (e.g., through biomolecule attachment or gas condensation on the sensor surface) the amount of surface concentration can be quantified by monitoring the reflected light intensity or tracking the resonance angle shifts. Typically, an SPR biosensor has a detection limit on the order of 10 pg mL\(^{-1}\) [167].

In this work, the combination of 1D SPR photonic crystal and the LBL assembled submicron silica particles is introduced [168]. The deposition of the silica spheres on the sensor surface creates the porous structure which covers homogeneously the sensitive area. Gases can condense according to three different mechanisms: in the air (homogeneous nucleation), on the surface (heterogeneous nucleation) and inside the pores. Taking into account that the gas condensation in the pores occurs at the lowest partial gas pressures [127], the designed functional coating allows increasing the detection limit of the modified SPR sensor. The development of a sensor is based on silica spheres of various diameters, as well as of different nature - hydrophobic and hydrophilic. The detection is based on measuring the parameters of the sensitive layer, such as the refractive index and thickness, of a layer consisting of silica particles and condensed gases.

4.2 Experimental section

4.2.1 The structure of the photonic crystal

The 1D photonic crystal consists of alternating Ta\(_2\)O\(_5\)/SiO\(_2\) layers deposited onto a silica substrate. The detailed parameters of fabricated samples are as follows. The widths of SiO\(_2\) layers in the photonic crystal are 270 nm and Ta\(_2\)O\(_5\) layers - 155 nm plus the most
external additional waveguide SiO$_2$ layer with a thickness of 370 nm. The widths of all layers, as well as the number of pairs of alternating layers, see Figure 4.1.

![Diagram](image)

*Figure 4-1: The scheme of the photonic crystal providing the resonance at 780 nm.*

The concrete values were selected to optimize the ultralong surface plasmon propagation conditions for the case when the structure is exposed to laser radiation at 780 nm. Hydrophilic and hydrophobic silica submicron particles were deposited on the waveguide layer, creating a developed surface and promoting the adsorption of matter on the waveguide layer of the photonic crystal, which makes it sensitive to the presence of water vapor and gases of different nature contacting with the sensor.

The described structures are designed in such a way that the waveguide mode can be effectively excited in the silica waveguide layer, and due to the small thickness of this layer (370 nm), the electromagnetic field of this mode is quasi-surface in nature, thus, it effectively penetrates the adsorption-selective layer, providing high resonance sensitivity to changes, associated with the adsorption or condensation onto the sensor surface. Therefore, the center of resonance associated with the excitation of the waveguide mode shifts along the wavelength and angle.
4.2.2 Calibration of fabricated structures

The experimental setup comprises the laser diode, the plasmonic heterostructure (1D photonic crystal) placed onto the BK-7 glass prism and the CMOS matrix. Laser light is focused onto the crystal surface in such a manner that the central angle of incidence corresponds to the resonant surface plasmon excitation angle in the Kretschmann scheme. Angular interrogation is used: light reflected from the heterostructure surface forms a divergent beam which without any focusing is detected by the CMOS matrix.

![Schematic representation of the experimental setup.](image)

After fabrication, the photonic crystals were tested without silica porous coating with water \((n = 1.33)\) covering the whole sensor surface. It allowed to measure the reflectance spectra and to determine the structure quality itself, without the influence of the possible differences in silica coating quality. All 8 fabricated photonic crystal structures showed equally good resonances under the illumination of 780 nm laser light (Figure 4.3).
Figure 4-3: Reflectance spectra of 8 fabricated PC samples. The same shape denotes equal sensitivity of the samples.

Some small shifts observed for experimental curves corresponding to different samples are due to the changes of the experimental conditions (temperature, surface cleaning quality, etc.) rather than due to the difference in the structures themselves. All curves have the same angular width that corresponds to nearly equal sensitivity of the photonic crystal-based structures. The oscillatory angular pattern implies that in the absence of the nanoparticle coating, the excited quasi surface wave is long-range propagating. The origin of such a pattern is the interference of the light, reflected from the structure and the light, transferred in the quasi surface mode, and then coupled back via prism to radiation propagating collinearly to the reflected light.
4.2.3 Silica particles coating on the surface of photonic crystal

Deposition of the hydrophilic silica particles onto the surface of photonic crystals ensures the creation of the porous functional layer supporting condensation of water and water-soluble gases at the lower partial gas pressures comparing to planar (smooth) surface. Silica particles form the pores at two interfaces which are the particle-particle and particle–photonic crystal contact (Figure 4.4).

![Figure 4-4: Area of analyte condensation between 180 nm particles and substrate (under normal conditions).](image)

The important thing is the analysis of the effect of particle size on the amount of condensed gas (the volume of recovered liquid). For this study, the volume of condensed analyte into pores between particles and substrate was calculated for silica particles of different sizes (available after the synthesis). A total amount of condensed analyte per unit area was calculated using the equation (Eq. 4.1):

\[
V_{\text{total}} = N_{\text{particles}}(V_1 + V_2)
\]

where \(V_{\text{total}}\) - the total volume of the condensed analyte, \(N_{\text{particles}}\) - number of particles per unit of area, \(V_1\) - volume of condensed analyte between particles, \(V_2\) - volume of condensed analyte between the particle and the substrate (photonic crystal).

It has been found, that the total amount of condensed analyte between 180 nm particles and the substrate is 1.6 times higher than one between 300 nm particles and
substrate. Based on the obtained data and possible particle variants, silica particles with a diameter of 180 nm were chosen as optimal for further experiments.

The formation of silica coating onto the surface of photonic crystals consists of three main stages: sample cleaning, preparation of the substrate, adsorption of silica particles. The deep coating method (Figure 4.5) has been chosen due to its versatility, reproducibility and simplicity.

At the cleaning stage, it was shown that for effective cleaning of the crystal, it is necessary to treat with an acid solution, alkaline, as well as a mixture of organic solvents (toluene, acetone, alcohol). Next, the crystal is processed in plasma for 1 minute on each side (longer processing is not possible due to the instability of the coating of the photonic crystal). For adsorption of hydrophobic silica particles, the surface of the photonic crystal needs the pre-hydrophobization.

The morphology of the resulted hydrophilic and hydrophobic surfaces is presented in Figure 4.6. It can be seen from the SEM images that the hydrophobic coating is more uniform than the hydrophilic one. Optical measurements based on the produced structures are provided in the next section.
4.2.4 Optical characteristics of water condensation on the sensor surface

The gas circulation setup contains a sealed chamber made from poly(methyl methacrylate), a membrane pump, and fitting for optical gas sensor. These units are connected by silicone tubes. The commercially available humidity meter (Center 311 rs 232, Center Technology corp.) has been used for temperature and humidity monitoring. The schematic of the experimental setup is illustrated in Figure 4.7.

To demonstrate the sensing capability of the produced structures, the response to both water condensation and changing humidity has been recorded for the photonic crystals functionalized with hydrophilic and hydrophobic silica particles.
As can be seen in the graphs, the response to humidity changes is different for the photonic crystals coated with silica particles of different nature (Figure 4.8).

**Figure 4-8**: Dependence of reflection on an angle for (a) – hydrophilic and (c) – hydrophobic coatings.

The hydrophilic system has been shown to detect changes in humidity. It was established, that responses to humidity are significantly higher for hydrophilic particles in comparison with hydrophobic one.
4.3 Summary

In this chapter, the development of the one-dimensional photonic crystal-based gas sensor has been described. The functional coating of the designed structure was fabricated by silica submicron particles of different nature - hydrophobic and hydrophilic ones. The detection is based on measuring the amount of condensed gases in the pores formed by silica particles on the sensitive area of the photonic crystal. Gases can condense according to three different mechanisms: in the air (homogeneous nucleation), on the surface (heterogeneous nucleation) and inside the pores [169]. Condensation in the pores occurs at the lowest partial gas pressures. The size of the silica particles defines the size of the pores which, in turn, is responsible for the amount of the condensed gases inside. It has been shown, that the total amount of condensed analyte between 180 nm particles and the substrate is 1.6 times higher than one between 300 nm particles and substrate.
5. Chapter 5. Postmodification of functional nanocoating

5.1 Introduction

Novel modalities of hybrid optical fibers typically come with increased optical losses since a significant surface roughness of functional layers gives rise to additional light scattering, restricting the performance of functionalization. For a deposition with a constant thickness increment, the surface roughness increases with the overall number of layers [14,118]. Thus, after substantial height variation, the rough coating appears extra light scattering due to surface topologies on the order of the wavelength of light that results in additional waveguiding losses that are unwanted in some applications based on optical properties of functional coatings [118]. To this extend, postmodification of multilayer films may result in the appearance of novel structures or advantageous structural changes in the film. The surface morphology of polymer layers is usually controlled through postprocessing by “annealing” in aqueous solutions of different salt concentrations or pH levels. By controlling pH and ionic strength, it is possible to vary the thickness of adsorbed layers from ~1 to ~10 nm or, in some cases, completely prevent the multilayer deposition process [107,119]. Several research groups showed that treatment of polyelectrolyte multilayers in salt solutions caused swelling and led to smoother surfaces showing faster annealing for higher salt concentrations [118,120]. Treatment of multilayers with solutions at varying pH-induced morphological irreversible and reversible changes in both weak polyelectrolyte [101,119] and in H-bonded multilayers [121,122]. The intrinsic property of multilayers composed of weak polyelectrolyte complexes is that they can be destroyed at extreme pH conditions, as the pH-induced imbalance of charges overcompensates the attractive polymer-polymer ionic binding [123].

Another problem is that the conventional strategies rely on using materials with poor biocompatibility and high toxicity which are not optimal for sensitive in vivo applications.

5.2 Motivation

Here, a novel type of ultrasmooth, biocompatible and removable functional nanocoating for HC-MOFs formed by LbL assembly of bovine serum albumin (BSA) and
tannic acid (TA) is introduced. The mechanism of the film deposition is based on the natural ability of tannins to precipitate proteins through hydrogen bonding and hydrophobic interactions [170].

Being the most abundant blood plasma protein, BSA is fully biocompatible [171]. In turn, the presence of galloyl groups [172] supplies TA with anti-inflammatory, antibacterial, antioxidant, and antifouling properties [172–174] that is extensively used for treating many diseases, tissue engineering [175], and wound healing [176]. Thus, functionalization with BSA/TA multilayers opens for HC-MOFs promising perspectives for using in in vivo biophotonic applications, including neurophotonics and biosensing.

The important benefit of the sequential LbL deposition technique is its versatility and cost-efficiency. The film formation occurs in the water at ambient temperature and does not require any special equipment and expensive material components. Although cheap and simple, this entirely aqueous-based automotive process creates multifunctional self-assembled films engineered at the nanoscale accuracy in a highly controllable, reproducible and reliable way.

5.3 Experimental section

For the creation of BSA/TA functional multilayers on the inner surface of HC-MOF, the modified version of the coating setup (Figure 3.4) has been used with connected suppliers of BSA and TA solutions. Solutions of BSA, TA and pure deionized water are streamed successively through the fiber by a peristaltic pump until the desired number of BSA/TA bilayers is formed. The pump creates a controllable and persistent liquid flow through the fiber, and the coating is formed by hydrophobic interactions and hydrogen bonding of protein-phenolic complexes at a neutral condition (pH 7) [112,170,177].

Morphology of the resulted coating is investigated via statistical analysis of 10 SEM micrographs for the fiber cross-sections taken at various positions along the fiber (Figure 5.1).
Figure 5.1: Evaluation of the coating roughness and thickness. (a) and (b) The structure of 8 BSA/TA bilayers before and after the alkaline treatment across the fiber cross-section. (c) The structure of 18 BSA/TA not-etched bilayers along the fiber. The frame color corresponds to the position where the SEM images were taken. The initial length of all the fibers was 6 cm, then three equidistantly located cuts were taken.

The substrate thickness as a function of the number of bilayers is well described by a linear fit with the slope of 5.2 ± 0.3 nm per bilayer (Figure 5.2a,b). To gain insight into this result, one should account for an ellipsoidal structure of BSA molecules with dimensions 4 nm x 4 nm x 14 nm in an aqueous solution which alongside 1-nm-thick TA molecules is expected to yield a BSA/TA bilayer as thick as ~5 nm for a side-on alignment and ~15 nm for an end-on alignment [178]. At pH 7 both BSA and TA molecules keep negative charges so that the formation of BSA/TA complexes is driven by hydrogen bonding and hydrophobic interactions only [112]. Hence, a side-on scenario is more likely in the considered case, and it is clearly confirmed by the abovementioned evaluation of the bilayer thickness. Additionally, this evaluation is in good agreement with previously published data for the LbL coating of planar substrates, where the thickness per BSA/TA bilayer formed at pH 7 was ~7 nm [112].
Figure 5-2: Characterization of the BSA/TA coating. (a) SEM micrographs of BSA/TA multilayers (indicated by the pseudocolor) before and after the etching. The coating (b) thickness and (c) roughness before etching as a function of the number of bilayers. The coating (d) thickness and (e) roughness versus the treatment time. The coating thickness is evaluated from SEM images (bars) and the shifts in the fiber transmission windows (red points). Error bars denote the coating roughness. The linear fit in (b) corresponds to the thickness of 5.2 nm per single bilayer. The coating roughness in (e) is fitted by the exponential function with the initial roughness $R_0 = 25.9$ nm and the decay time $\delta t = 2.2$ min.

Finally, SEM micrographs show that BSA/TA coating is formed in the internal surface of the central capillary only even though injection of the solutions is performed in all fiber capillaries. This effect is attributed to the enormous difference in the hydraulic
resistance of the central and side capillaries. In the framework of the Hagen–Poiseuille model [179], the capillary hydraulic resistance is inversely proportional to its radius to the fourth power that means that a flow rate in the side channels is at least 1000 times slower than in the core channel (see the detailed fiber geometry in Figure 3.1). The capillary hydraulic resistance can be expressed as:

\[ R = \frac{8 \mu L}{\pi r^4} \]  

(5.1)

where \( \mu \) is dynamic viscosity, \( L \) is capillary length, \( r \) is the capillary radius.

For this reason, the coating is formed on the inner surface of the central capillary mostly. The coating formation in the side capillaries is possible but its thickness is less than the minimal structures of BSA/TA that SEM can resolve on the glass substrate (\(~10\) nm) [14,94] which almost does not affect its optical properties.

Figures 5.2a and 5.2c show that the coating roughness increases with a growth in the number of bilayers, reaching 25 nm for a 140-nm substrate (28 bilayers). This is a general property of the LbL-deposited substrates, leading, specifically, to a significant rise in the fiber optical losses. To smooth the BSA/TA coating, we use its high sensitivity to the alkaline pH level of the ambient media, reducing protein binding accompanied by the coating dissociation [180]. Specifically, we post-process the coated samples by injection of the aqueous solution of NaOH at pH 9. Figures 5.2d and 5.2e show the evolution of the coating topography in the time when the initial structure is formed by 28 BSA/TA bilayers. Importantly, while the coating thickness decreases almost linearly, the roughness manifests an exponential decay as \( R = R_0 \exp(-t/\delta t) \), where \( R_0 = 25.9 \) nm is the initial roughness and \( \delta t = 2.2 \) min is the roughness decay time. Hence, the smoothing is performed much faster than the dissolution which is also confirmed by the SEM images of multilayers with close thicknesses before and after the post-processing (Figure 5.2a). Finally, we reach the roughness of 3 nm at the substrate thickness of 30 nm that is 7 times smaller than the roughness of the initial substrate with the same thickness (Figure 5.3).
To describe the optical properties of the BSA/TA multilayer, we employ the effective medium approximation within the Bruggeman formulation which introduces the effective permittivity of a two-phase mixture $\varepsilon_{\text{eff}}$, in the assumption that TA molecules in the form of spherical inclusions are randomly located in a homogeneous environment formed by BSA, as follows [181]

$$\frac{(1 - f_{TA}) \varepsilon_{\text{BSA}} - \varepsilon_{\text{eff}}}{\varepsilon_{\text{BSA}} + 2\varepsilon_{\text{eff}}} + f_{TA} \frac{\varepsilon_{\text{TA}} - \varepsilon_{\text{eff}}}{\varepsilon_{\text{TA}} + 2\varepsilon_{\text{eff}}} = 0,$$

(5.3)

where $\varepsilon_{\text{TA}}$ and $\varepsilon_{\text{BSA}}$ are permittivities of TA and BSA, and $f_{TA}$ is the volume fraction of TA. Taking into account that $\varepsilon_{\text{TA}} = 3.71$ [182] and $\varepsilon_{\text{BSA}} = 2.25$ [14], we note that Eq. 5.3 still contains two unknown variables – $\varepsilon_{\text{eff}}$ and $f_{TA}$ – which leads to multiple possible solutions.

To resolve this issue, the HC-MOF transmission spectrum was calculated by the transfer-matrix approach, following Noskov et al. [40]. Taking into consideration the fiber geometrical parameters alongside the glass refractive index and the coating thickness extracted from SEM micrographs, we evaluate the coating effective permittivity through fitting the theoretical fiber transmission spectrum to the measured one and find that $\varepsilon_{\text{eff}} = 2.56$. Hence, Eq. 5.3 yields $f_{TA} = 0.24$ and, consequently, $f_{\text{BSA}} = 1 - f_{TA} = 0.76$. Importantly, these values are in a good agreement with 4-nm and 1-nm thicknesses of BSA and TA molecules forming a 5.2-nm single bilayer in a side-on alignment.
Deposition of the BSA/TA coating shifts the fiber transmission windows towards longer wavelengths (Figure 5.4a) (Eq. 2.12) because of the growth in $d$, albeit with increased optical loss caused mainly by the layer roughness [14]. On the contrary, pH-treatment dissolves the BSA/TA coating associated with the blue shift of the transmission windows (Figures 5.4b and 5.4c). The transmission spectrum is returned to the case of an uncoated fiber in 7 min of the etching when the substrate is fully removed.

Figure 5-4: Evolution of the fiber transmission spectrum (a) with growth in the number of BSA/TA bilayers deposited and (b) in time upon the alkaline treatment for
the HC-MOF coated with 28 BSA/TA bilayers. Relative shifts of the transmission maxima vs (c) the number of BSA/TA bilayers deposited and (d) the treatment time for the initial coating with 28 BSA/TA bilayers. The measured values are denoted by points joined with lines as guides for the eye.

Additionally, the alkaline etching gives rise to an exponential temporal decrease in the fiber loss with the decay time $\delta t = 4.1$ min (Figure 5.5a). It is important to note that the decreased fiber loss can be obtained for any predefined coating thickness. As an example, Figure 5.4b compares the fiber loss for not etched and etched samples, supplementing data on the coating morphology shown in Figure 5.2a. 2-min etching of HC-MOF with 28 bilayers decreases the fiber loss by $\sim40\%$ from 1.2 dB cm$^{-1}$ to 0.7 dB cm$^{-1}$ that is 30% less than the loss for the not-etched fiber with the equal coating thickness $\sim115$ nm. Furthermore, 4-min etching results in the loss drop by three times up to 0.41 dB cm$^{-1}$ with the coating thickness $\sim30$ nm and roughness $\sim3$ nm (see also Figure 2a).
Figure 5-5: Optical fiber loss as a function of (a) treatment time and (b) coating thickness. Fiber losses are calculated by averaging across minimal losses for all transmission windows, and the error bars correspond to the standard deviation. The substrate with 28 initial BSA/TA bilayers was etched. The fiber optical loss in (a) is fitted by the exponential function with the initial fiber loss $\alpha_0 = 1.16 \text{ dB cm}^{-1}$ and the decay time $\delta t = 4.1 \text{ min}$. The loss measurements were performed by the cut-back technique.

5.4 Summary

In summary, a novel type of functional nanocoating for HC-MOFs formed by LbL assembly of BSA and TA has been demonstrated. Tuning the HC-MOF transmission spectrum with the BSA/TA multilayers is a highly controllable and fully reversible operation. The resulted BSA/TA multilayers are characterized by the thickness of 5.2 nm per single bilayer with a surface roughness reaching 26 nm for the 140 nm thick layer. The average thickness per single bilayer has a good correlation with previously published data.
for planar layers [112]. To smooth the BSA/TA substrate, alkaline etching has been applied. The temporal kinetics of the coating dissolution shows that the alkali drops the surface roughness to 3 nm within 4 min of the treatment, resulting in decreasing the fiber optical losses by three times. The coating is fully removed in 7 min of the treatment.

The simplicity, speed, and efficiency make the presented technique stand out from other similar techniques of producing LbL-assembled multilayers from polymers whose smoothing calls for the time ranging from several hours to several days [118,120,183].

Additionally, full biocompatibility alongside anti-inflammatory and antibacterial properties makes it possible to implant HC-MOFs functionalized with BSA/TA multilayers into living tissue which could serve them as a promising neurophotonic interface providing enhanced light-neuron interactions for efficient optical manipulations of neuronal structures and monitoring brain functions [184]. Beyond that, TA-functionalized planar films have recently been found to efficiently capture circulating tumor cells (CTC) [172]. This suggests that, being incorporated into a medical endoscope, the considered system would potentially enable real-time monitoring of CTC in bodily liquids.
6. Chapter 6. In-fiber multispectral optical sensing

6.1 Introduction

The interaction mechanisms of light with tissues, cells and liquids are the basis for the most extensive development of novel optical methods for use in biology and medicine. These methods allow one to obtain information about the structure, state, and transformation of various components of biological systems [185]. The increasing medical need for robust techniques suitable for real-time diagnostics at the place of patient care is at the cutting edge of modern biosensing. Among the variety of available sensing devices, optical label-free sensors demonstrate high sensitivity to ambient refractive index variations, attracting considerable attention from the chemical, biomedical and food processing industries. The main efforts in the development of such sensors are focused on increasing refractive index sensitivity (RIS) through the employment of cavity resonances (including surface plasmon resonances, Mie resonances, whispering gallery modes, etc.) and propagating eigenmodes in dielectric and plasmonic nanostructures. Conceptually, another approach is realized by HC-MOFs, which allow sensing of liquid analytes by monitoring the changes in the transmission; HC-MOFs have a great advantage of enabling high volume for measuring light-analyte interactions, which improves the RIS in comparison to that with cavity-based counterparts.

6.2 Motivation

The refractive index of any biological liquid is a basic material parameter that characterizes how light interacts with liquids. Refractive index is a nonlinear parameter and strongly depends on wavelength, in the visible range, a decrease of the RI comes with an increase of the wavelength. This dependency is called optical dispersion [185]. In spite of the existence of comprehensive RI measuring systems and techniques, for many biological liquids and blood components, the data for RI in a wide spectral range and concentrations are not yet available or available only for a single wavelength [23]. In many optical studies, a rough estimate of RI of the biological liquids under study, based on the fact that the main constituent of any solution is water or more precisely a mixture of water and other materials, is often used. Therefore, these data are out of the majority of practical
use especially for optical diagnostics by using different lasers and at tissue heating in the course of various laser therapies.

However, monitoring of the RI in the broad spectral range act as a simple and cost-effective fingerprint of liquid biosamples to enable real-time analysis of changes in their composition. These features are also important to provide rapid diagnostics of pathological changes in cells, tissues and other biological samples. In particular, variations in the optical dispersion of blood serum may indicate some diseases since it is directly related to changes in blood components, specifically the concentration of albumin and the appearance of its conjugated forms. Recently, it was shown that variations in the blood serum RI could be used as an additional criterion in the analysis of antitumor therapy and RI monitoring for glycated hemoglobin and albumin enables diagnostics of type 2 diabetes and pre-diabetic status. Serum albumin is the most abundant blood plasma protein and plays a pivotal role in maintaining oncotic pressure as well as in transporting poorly soluble molecules, including lipid-soluble hormones, bile salts, unconjugated bilirubin and many others. The normal concentration of albumin in the serum of human adults is 35–54 g L$^{-1}$, while its deviations indicate various abnormal conditions and diseases. Since albumin is optically transparent, direct determination of the analyte concentration by measuring the optical absorption is not applicable. The typical detection of the albumin concentration is based on the changes in dye absorbance (such as bromocresol green or bromocresol purple) upon binding to albumin. Alternatively, it was proposed to detect low concentrations of albumin with the optical spring effect in an optomechanical oscillator and plasmon polaritons in a hyperbolic metamaterial. Such techniques, however, are time-consuming and do not allow instantaneous monitoring of albumin in biological fluids in real-time.

Here, the concept of in-fiber multispectral optical sensing (IMOS) for liquid biological samples in both static and real-time modes was introduced. The sensing principle relies on detecting spectral shifts of maxima and minima in the transmission spectrum of HC-MOF when a liquid bioanalyte is streamed through it via specially designed liquid chambers. These resonant features are associated with Fabry–Perot resonances in the core capillary wall, and their spectral positions are unambiguously related to the bioanalyte
refractive index. IMOS offers a unique opportunity to measure the refractive index at 42 wavelengths, with a sensitivity up to ~3000 nm per refractive index unit (RIU) and a figure of merit reaching 99 RIU\(^{-1}\) in the visible and near-infrared spectral ranges. We apply this technique to determine the concentration and refractive index dispersion for bovine serum albumin (BSA) and show that the accuracy meets clinical needs.

6.3 Results and discussion

6.3.1 Empirical extraction of RI for liquid filling

The validity of the proposed approach of IMOS was demonstrated by measurements of the RI for BSA at different concentrations dissolved in a water buffer. A single HC-MOF allows simultaneous measurement of an analyte’s RI synchronously at seven wavelengths (4 minima and 3 peak centroids) in the visible and near-infrared spectral domains. However, such a number of wavelengths is still insufficient for accurate retrieval of RI optical dispersion, especially in cases when data are contradictory or not available. The number of discrete wavelengths available for measuring RI can be increased by using several HC-MOFs with slightly shifted transmission windows with the help of six functionalized HC-MOFs with 0, 14, 22, 31, 40 and 54 PAH/PSS bilayers (see Section 3.4.4).

The measurements start with calibration of the system by recording the transmission of the water-filled fiber and associate the spectral positions of the minima and the peak centroids with the water RIs by using Eqs. (2.12) and (2.13). The stability of the experimental technique was confirmed by the excellent agreement of the measurements with the well-known optical dispersion of deionized water adopted from Ref. [186].

Figure 6.1 shows the transmission spectra of the liquid-filled HC-MOF with different concentrations of BSA solution (0 and 20 g L\(^{-1}\)). Optical dispersion of water is taken as a reference from Ref. [186] as follows (Eq. 6.1):

\[
\begin{align*}
n_{\text{water}} &= \sqrt{1 + \frac{0.5670093832 + \lambda^2}{\lambda^2 - 0.004610301794} + \frac{0.1719708856 + \lambda^2}{\lambda^2 - 0.019835060155} + \frac{0.01992501582 + \lambda^2}{\lambda^2 - 0.022241458096} + \frac{0.119965424 + \lambda^2}{\lambda^2 - 13.27505178}} \\
&= (6.1)
\end{align*}
\]
RI of the BSA-water solution can be extracted empirically by adding a correction ($\Delta n$) to $n_{water}$ to obtain coincidence in the positions of transmission minima and maxima (or maxima centroids) for theoretical (dotted green line) and experimental (solid green line) transmission spectra. The positions of the centroids have been found to be more sensitive to the variations in an analyte RI than the maxima and were used for further measurements.

**6.3.2 Transmission of HC-MOFs filled with a water-BSA solution**

In the static regime, HC-MOFs were integrated into a smart cuvette and filled by the solutions in the test through capillary action. Once the fiber was filled completely and no air bubbles appeared, the transmission spectrum was recorded successively for each fiber sample. In addition to fiber holding, the smart cuvette can also control meniscus formation that is important for light coupling when the fiber is filled with liquid. Each of the BSA-filled samples has four well-defined minima of the transmission spectra in the

---

*Figure 6-1: Theoretical and experimental transmission spectra of HC-MOF filled with water and the BSA-water solution at the concentration of 20 g L$^{-1}$ [14].*
visible spectral range (400 nm – 900 nm) while the peaks are distorted (Figure 6.2) and for that reason, we use the centroids of the transmission windows in the analysis.

![Image](image.jpg)

**Figure 6-2:** Static measurements of the transmission for HC-MOFs filled with a water-BSA solution. (a) The schematic of the optical setup. (b) The transmission of liquid-filled HC-MOF for different concentrations of BSA [14].

### 6.3.3 IMOS in static mode

Figure 6.3a shows the evolution of transmission spectra caused by an increase in BSA concentration in a water buffer. Using these data, we extract RIs by the same algorithm (Figure 6.4) as that for pure water filling and plot them along with the Sellmeier fits, as shown in Figure 6.3b. To verify our results independently, we also measure the RIs
of these samples by a multiwavelength Abbe refractometer (denoted by the stars in Figure 6.3b) and find very good agreement with the IMOS results.

Figure 6-3: Performance of IMOS for BSA dissolved in deionized water in static mode. (a) Transmission spectrum evolution with increasing BSA concentration for the non-modified HC-MOF. (b) Optical dispersion of BSA in a water buffer with different concentrations. The colored points indicate the RI values extracted from the shifts in the minima and the peak centroids of the fiber transmission spectra, and the solid lines mark their Sellmeier fits. For pure water, the Sellmeier fit describes the water dispersion adopted from Ref. [186]. The error bars are obtained from the spectrometer’s optical resolution. The stars mark RIs measured by the Abbe refractometer, provided for comparison [14].
Figure 6-4: Algorithm for the extraction of optical dispersion of BSA solution at different concentrations.
In practical applications, it is important not only to determine the RIs of a biological liquid but also to quantify the concentration of target biomolecules. To this end, we calibrate our system by associating the RIs of the samples at different wavelengths with the concentration of BSA (Figure 6.5). Since the concentration of BSA is quite low, these dependencies are linear.

**Figure 6-5: Calibration relating the concentration of BSA and RIs of the BSA-water solution at different wavelengths. The RIs of BSA are extracted from the Sellmeier fits of the experimental points [14].**

### 6.3.4 Impact of the liquid sample internal losses on the HC-MOF transmission

However, it should be noted that solutions with strongly absorbing analytes can be investigated only with preliminary preparation of the probe via dilution. The higher optical losses introduced by the low-transparency filling media result in minima and maxima distortion. Increasing optical losses of the sample will lead to eroding the maxima and minima of the fiber transmission spectra, deteriorating the IMOS performance. Figure 6.6 provides quantitative evaluations, showing the transmission spectra of a 6-cm-long fiber for various imaginary parts of the sample refractive index ($n''$). Importantly, while the maxima are well distinguished up to $n'' = 0.01$, the minima get markedly eroded for longer wavelengths at $n'' \geq 0.001$. Thus, IMOS is best performed for sufficiently transparent liquids.
108

Figure 6-6: Fibre transmission spectra for a various imaginary part of the sample refractive index: 0 (black), 0.0005 (cyan), 0.001 (blue), 0.005 (red) and 0.01 (magenta). The real part of RI equals to 1.33 [14].

6.3.5 Refractive index sensitivity and figure of merit

The key characteristics of label-free optical sensors are the RIS, defined as the ratio of the change in sensor output (the shift of the resonant wavelength) to the analyte RI variation, and the figure of merit (FOM), which normalizes the RIS to the width of the tracked resonance characterized by the full width at half maximum (FWHM). Figure 6.7 shows the transmission minima as a function of analyte RI along with RIS and FOM. The slope of the linear fit corresponds to RIS as (Eq. 6.2):

\[ RIS = \frac{\Delta \lambda}{\Delta n} \]  \hspace{1cm} (6.2)

FOM is RIS normalized by FWHM of a resonance (Eq. 6.3):

\[ FOM = \frac{RIS}{FWHM} \]  \hspace{1cm} (6.3)

Using the fiber transmission spectra (Figure 6.3a) and the determined RIs of the BSA-water solutions (Figure 6.3b), the transmission spectra minima versus the analyte RI were plotted. The slopes of the linear fits show the RIS of the MOF-based sensor, which varies from 1100 nm RIU\(^{-1}\) for the blue light to 3000 nm RIU\(^{-1}\) for infra-red light. The
corresponding FOM varies from 60 to 99 RIU\(^{-1}\). These values along with the working spectral range are typical for surface plasmon and 2D material sensors. However, the proposed approach provides a great benefit of multispectral analysis in a broad spectral range.

Figure 6-7: (a,b,c,d) The minima positions extracted from the transmission spectra of HC-MOFs as a function of the filling refractive index obtained by variations in the concentration of BSA. The error bars are smaller than the data points [14].
6.3.6 Optical dispersion of refractive index for bovine serum albumin

It is important to note that the optical dispersion for a solution containing an investigated substance dissolved in a water buffer can be used to determine the optical dispersion of the pure product. Such a possibility is of special interest in cases when the substance of interest is difficult to synthesize in the form of thin films, which are normally suitable for analysis with standard techniques such as ellipsometry or refractometry. This is the case for BSA, whose RI has been reported for only a few wavelengths: 436 nm [187–190], 546 nm [187,188,190], 578 nm [190–192], 589 nm [187,192], and 840 nm [193].

Accounting for BSA molecules as uniaxial ellipsoids with overall dimensions of 4 nm x 4 nm x 14 nm [194,195], the extraction can be performed by using the effective medium approximation, which describes the effective permittivity $\varepsilon_{\text{eff}}$ of the solution by the Maxwell Garnett equation as follows (Eq. 6.4) [181,196]:

$$
\varepsilon_{\text{eff}} = \varepsilon_e + \frac{f_{\text{BSA}}}{3} \sum_{j=x,y,z} N_j (\varepsilon_i - \varepsilon_e) - \frac{\varepsilon_i - \varepsilon_e}{1 - f_{\text{BSA}} (\varepsilon_i - \varepsilon_e) \sum_{j=x,y,z} N_j (\varepsilon_i - \varepsilon_e)}
$$

(Eq. 6.4)

where $\varepsilon_e$ and $\varepsilon_i$ are the permittivities of the water buffer and the inclusions (BSA molecules), respectively, $f_{\text{BSA}}$ is the volume fraction of the BSA molecules, and $N_x$, $N_y$ and $N_z$ are the depolarization factors over the x, y and z axes, respectively. The molecular weight of 66.5 kDa [194,195] and dimensions of BSA molecules allow us to translate the mass concentration of BSA into the volume filling factor $f_{\text{BSA}}$. By using the known optical dispersion of water and the measured RIs of the BSA-water mixtures, we determine the optical dispersion of BSA (Figure 6.8). To verify the repeatability of this process, we perform this procedure for 3 concentrations of BSA, 20 g L$^{-1}$ ($f_{\text{BSA}} = 0.0213$), 40 g L$^{-1}$ ($f_{\text{BSA}} = 0.0425$), and 60 g L$^{-1}$ ($f_{\text{BSA}} = 0.0638$), resulting in almost identical dispersion curves. The discrepancy falls within the range of the measurement accuracy.
Figure 6-8: The refractive index of BSA determined via the Maxwell Garnett approximation. Points correspond to the measurements of RI for BSA-water, and solid lines mark the Sellmeier fits. The extraction was performed for 3 concentrations of BSA to show the repeatability of the result [14]. The error bars are smaller than the marker size. The stars mark BSA RI values adopted from Refs. [187–191,193].

It is instructive to compare the RI dispersion of BSA obtained by IMOS with the data available in the literature [187–191,193] (Figure 6.8). All previous measurements of BSA RI have been performed by refractometry of water-BSA solutions, and they show deviations from each other and from our results. However, the difference between the results is in the range of less than 0.025 RIU. These dissimilarities can be attributed to the distinct purity of BSA used in different measurements. In the current experiments, BSA produced by Sigma-Aldrich with a purity above 96% was utilized, while the purity of BSA measured in previous works was not reported. However, purity is a critical parameter that can significantly affect the measurement results. To this end, we compare the results for BSA produced by Sigma-Aldrich (>96% purity) [197] (St. Louis, MO, USA) and Agat-Med (50% purity) [198] (Moscow, Russia) and find a discrepancy of ~0.05 RIU (Figure 6.9). The purity of the samples has been verified by sodium dodecyl sulfate-polyacrylamide gel electrophoresis analysis.
Figure 6-9: The refractive index of BSA extracted via the Maxwell Garnett approximation. Circles correspond to the measurements of RI for the BSA supplied by Sigma-Aldrich (>96% purity) and triangles to the BSA supplied by Agat-Med (50% purity), and solid lines mark the Sellmeier fits. The extraction is performed for 3 concentrations of BSA to show repeatability of the result [14]. The pentagrams mark BSA RI extracted from Refs [187–190,193,199].

6.3.7 IMOS in real-time

In the dynamic regime, HC-MOFs were sealed in specially designed liquid cells (LCs). Cells were prepared using the commercially available 3D printer Prusa i3 steel. Its printing tolerance of ~0.1 mm totally meets the accuracy requirements for the reproducible production of high-quality liquid cells. In total, two liquid cells and HC-MOF sealed in them form a simple and robust structure. A detailed schematic of the designed LCs is illustrated in Figure 6.10.
Liquid samples were streamed through the HC-MOFs by the peristaltic pump connected to the inlet of the LC. Real-time tracking of the transmission spectra minima was achieved by means of LabVIEW software (Figure 6.11).
measurement of the transmission spectrum. The red rays illustrate the light path from a broadband halogen lamp through the HC-MOF to the spectrometer and the CCD (charge-coupled device) camera to record the output mode profile. The insets depict the input and output spectra for different concentrations of BSA dissolved in PBS [14].

Figure 6.12 displays the results. Although the PBS buffer for BSA dissolution prevents the intensive formation of air bubbles while the analyte flows through the fiber, bubbles still appear at the moments of solution switching, leading to instantaneous disturbance of the minima positions during the transitional time intervals (colored curves in Figure 6.12).

Figure 6-12: IMOS in real-time for BSA dissolved in PBS buffer. The colored lines denote instantaneous positions of the transmission minima when the peristaltic pump is switched between 5 solutions with different concentrations of BSA. The black lines
exhibit the data smoothed with MATLAB. The flow rate created by the peristaltic pump is fixed at 1 mL min$^{-1}$ [14].

It should be noted that real-time monitoring of RI optical dispersion simultaneously at 42 (or even several hundred) wavelengths can be achieved by using several post-processed HC-MOFs with necessary modifications of LCs and adaptation of the optical setup to parallel measurements (Figures 6.13).

![Diagram](image)

Figure 6-13: Illustration of the automatic fiber switching in the system optical path by a piezo stage. Independent optical paths can be created to perform measurements simultaneously with all fibers [14].

6.4 Summary

In summary, the technique of IMOS based on the analysis of spectral shifts in the minima and maxima of the HC-MOF transmission filled with a bioanalyte has been proposed and experimentally demonstrated. In contrast to conventional optical biosensors that work at only a single wavelength, the presented approach allows simultaneous measurement of the RI at many wavelengths in the visible and near-infrared spectral domains with RIS values up to $\sim$3000 nm RIU$^{-1}$ and FOMs reaching 99 RIU$^{-1}$. Specifically, we have demonstrated the use of IMOS to measure the optical dispersion and concentration of BSA dissolved in water and PBS buffers in both static and dynamic regimes, with a resolution of $\sim$1 g L$^{-1}$ when determining the BSA concentration, which matches the accuracy of the standard tests on albumin. Furthermore, for the first time, to our knowledge, we have extracted the RI of pure BSA at 42 spectral points in the wavelength range 400–850 based on a specially developed algorithm (Figure 6.4). Potentially, the number of wavelengths available for the measurement of RI can be
increased further to several hundred by producing the necessary number of HC-MOFs with slightly shifted transmission windows [14].

It is instructive to compare IMOS with refractometers and ellipsometry, which perform similar RI identification. The operational principle of conventional Abbe refractometers relies on using a set of filters, one filter per single acquisition wavelength so that the RI measurements can be performed in a static regime only, and the number of wavelengths available for the measurements is restricted by the number of filters. Modern digital refractometers are more convenient, performing all operations in an automatic mode; however, they do not support real-time measurements. In-line refractometers, which are widely used in various manufacturing areas, target only a single wavelength (usually 589 nm) and therefore cannot be used for the laboratory analysis of liquids over a wide spectral range. Overall, the modern market of available refractometers is diverse. However, these devices are expensive, restricted in the number of wavelengths available for measurement (typically less than 10) and cannot perform real-time measurements at several wavelengths in parallel [200].

Thus, the main benefits of IMOS in comparison to refractometers and ellipsometers are simplicity and cost efficiency, and the setup is quite compact and simple for reproduction. In addition, IMOS makes it possible to perform RI measurements over a wide spectral range, providing great capacity for practical use. Specifically, the integration of LCs with surgery endoscopes will pave the way towards the intraoperative analysis of bodily fluids, enabling surgeons to act in a timely manner under variable conditions. Multispectral analysis of saliva, urine, and ascitic fluid will facilitate diagnostics of various diseases. In addition, IMOS enables accurate determination of the RI optical dispersion for various proteins and their complexes, which is important for reliable simulations of biological processes [201].
7. Chapter 7. Noncontact characterization of microstructured optical fibers coating in real-time

7.1 Motivation

Various experimental techniques such as scanning electron, surface force and atomic force microscopy (SEM, SFM and AFM), X-ray and neutron reflectivity, UV-VIS and IR spectroscopy, single particle light scattering, ellipsometry, surface plasmon resonance (SPR), interferometry and quartz crystal microbalance (QCM) have been used to characterize self-assembled polyelectrolyte (PE) films [114,148,202–210]. Although these studies have yielded detailed information on the film thickness and properties, they are based on sophisticated measuring techniques using bulk and expensive laboratory tools that prevent fast and easy analysis of deposited layers. Moreover, most techniques operate only in a steady mode and are carried out on dried films, not allowing in situ monitoring of multilayer growth. The real-time ellipsometry, SPR, AFM and QCM measurements, in turn, require complicated calibration protocols and precise adjustment of measuring units, and they are very sensitive to the surface imperfections and any height deviations [203,209]. In addition, these methods are only suitable to characterize PE multilayers deposited on planar silicon and quartz substrate or a metalized surface. Interferometric reflectance spectroscopy is also applicable for very limited structures generating a fringe pattern [202]. The existing fiber-based sensing platforms realized on the geometry-modified fibers, such as long period grating (LPG) and tilted fiber Bragg grating (TFBG), suffer from poor mechanical stability and complicated fabrication process [10,132,211]. Therefore, currently, there is no technique allowing noncontact characterization of the fiber coatings in situ. SEM analysis of LbL functionalized MOFs has been found as the only reliable method for the estimation of coating thickness of the geometrically confined fiber surface [14]. However, since most of the commercial fibers are made of silica and its counterparts [212], an extra deposition of conductive metals required for the proper imaging decreases the contrast between fiber walls and functional coating and does not allow resolving nanometer-thin films [14]. Overall, there is a strong demand for real-time
monitoring of the coating growth during the self-assembly on the fiber surface. In this contribution, a new technique that resolves this issue has been demonstrated.

7.2 Results and discussion

The holey structure of HC-MOFs supports the simultaneous flow of aqueous solutions and light guidance in the water-filled core. We have succeeded in the growing of LbL PE films consisted of PAH and PSS inside the HC-MOFs and synchronous tracking of the shifts in the position of optical resonances correlating with the thickness of the deposited coating. An increase in the film thicknesses with increasing ionic strength in the PE solutions was experimentally observed for the coatings formed by three PAH/PSS bilayers assembled from the buffers containing 0.15 M and 0.5 M of NaCl [14]. The versatility of the HC-MOF-based platform for monitoring the pH-induced dissolving of nanocoating consisted of BSA and TA was demonstrated as well.

7.2.1 Experimental realization

The experimental analysis of the coating thickness relies on the transmission spectra measurements and tracking the position of optical resonances of liquid-filled HC-MOFs at each stage of multicycle assembly. An optically coupled optofluidic module is illustrated in Fig. 1. Liquid filling of fiber capillaries is obtained by inserting the tips of HC-MOFs into small liquid cells (LCs) equipped with tubing interfaces and optically accessible windows. Such a system ensures stable and reproducible measurements at different pumping rates from 100 to 1000 mL min$^{-1}$ [14]. A peristaltic pump (Shenchen LabV1) connected to the inlet of the LC creates the flow of applied solutions through the fiber. Microscope objectives (Olympus, 10x) are used to couple the light from a halogen lamp (Thorlabs SLS201L) into the fibers and to collect the transmitted signal. The output spectrum is analyzed at each step of LBL deposition process and measured with a spectrometer (Ocean Optics QE Pro). The custom algorithm in LabVIEW allows real-time tracking the spectral positions of minima in the fiber transmission spectra that are related with the coating thickness. Eq. 2.13 provides a convenient link between the position of the dips in the fiber transmission for the fundamental fiber mode only and the thickness of the assembled coating once the coating refractive index is close to the glass refractive index.
7.2.2 *In-situ* monitoring of coating buildup

To demonstrate the feasibility of the proposed technique for the dynamic analysis of different coating performance, the thickness of assembled PAH/PSS films dissolved in buffers containing 0.15 and 0.5 M NaCl were compared. The position of optical resonances for the water-filled non-modified HC-MOF serves as a reference for the following extraction of the coating thickness (Figure 7.1).

![Figure 7.1](image)

**Figure 7-1:** (a) Comparison of the experimental and theoretical transmission spectra for the water-filled non-modified and coated by the PEs dissolved in a buffer containing 0.15 M NaCl HC-MOF. The theoretical plot was obtained by adjusting the thickness of the polymer coating as 18 nm per 3 PAH/PSS bilayers. (b) The spectral evolution of the transmission minima associated with LbL assembly. The colour lines indicate instantaneous positions of the transmission minima when the peristaltic pump is switched between PE solutions and deionized water (w). The black lines exhibit the data smoothed with MATLAB.

The thickness of fiber coating is evaluated via adjustment of the coating thickness in the theoretical model to get a coincidence with the experimental transmission spectrum (Figure 7.1a). The polymer coating is included into the theoretical model as an additional
concentric layer of equal thickness on the core capillary [14]. For a coating consisted of 3 PE bilayers formed in the buffer containing 0.15 M NaCl, the spectral shifts of optical resonances were 5, 6, 7 and 9 nm for various minima in fiber transmission (Figure 7.1b) that corresponds to the formation of polymer coating with a thickness of 18 nm, which has been also verified by SEM (Figure 7.2b).

Figure 7-2: SEM micrographs of the core capillaries functionalized with 3 PAH/PSS bilayers in the presence of (a) 0.5 and (b) 0.15 M NaCl, respectively. (c) Coating thickness vs the number of PE bilayers. The coating thickness is evaluated from the shifts in the fiber transmission windows (points). Lines correspond to the thickness of 5.8 nm (0.15 M NaCl) and 10.6 nm (0.5 M NaCl) per single bilayer.

An increase in the film thicknesses with increasing ionic strength in the PE solutions from 0.15 to 0.5 M NaCl was observed. The higher salt concentration changes the molecular conformation from the linear to the globular or coiled structure. Thus, for a polymer coating consisted of 3 PAH/PSS bilayers formed in the buffer containing 0.5 M NaCl, the spectral shifts of optical resonances were 8, 12, 13 and 17 nm for various minima. This, in turn, corresponds to the formation of a 32-nm PE film on the inner surface of HC, confirmed by SEM (Figure 7.2a).

Hence, the average thickness increase of 6 ± 1 and 11 ± 1 nm per bilayer was extracted for the PE solutions in the presence of 0.15 M and 0.5 M NaCl, respectively (Figure 7.2c) [14]. These results are in good agreement with the postdeposition analysis based on transmission spectra measurements of dried functionalized HC-MOFs proving
the accuracy of *in situ* characterization of LbL assembled films. Thus, the proposed technique for the evaluation of coating performance can be a promising alternative to the existing methods applied for the thickness analysis of the sequentially assembled multilayers. In particular, to SEM micrographs which are suffering from a poor contrast between the deposited films and fiber surface that does not allow to resolve the nanometer-thin films (Figure 7.2a,b).

SEM micrographs show coating formation on the internal surface of the central capillary only despite solution injection in all fiber capillaries. This effect can be explained by the enormous difference in the hydraulic resistance of the central and side capillaries. The Hagen–Poiseuille model [179] states that the capillary hydraulic resistance is inversely proportional to its radius to the fourth power that means that a flow rate in the side channels is at least 1000 times slower than in the core channel for our fiber. Thus, for the typical coating deposition duration (~10-60 min) the film is formed on the inner surface of the central capillary only.

**7.2.3 In-situ monitoring of coating disintegration**

Finally, we demonstrate the performance of our technique for real-time monitoring of the coating dissolving. We employ BSA/TA complex as a coating since it was demonstrated that the binding inside this composite is very sensitive to the pH level of the surrounding media [180]. Thus, the solutions at low (acidic) and higher (alkaline) pH prevent and/or partially reduce protein binding and induce the dissociation of existed BSA/TA networks.

The adsorption of the BSA/TA multilayers leads to a slight red-shift while pH-annealing, in turn, induces the blue-shift of optical resonances due to the disintegration of BSA/TA coating from the cladding ring [132]. Figure 7.3 summarizes the coating evolution and the associated spectral shift of transmission minimum during the immersion with the alkalic solution at pH 9 and pH 11 for the fibers functionalized with 4 and 8 BSA/TA bilayers. The pump flow rate was set to 150 μL min⁻¹. The longest wavelength transmission minimum (Min 4) has been chosen for the study since it possesses the highest sensitivity to the thickness variations (Eq. 2.13).
Figure 7-3: (a) SEM micrographs of the uncoated fiber and the fiber functionalized with BSA/TA multilayers followed by the alkaline treatment. (b) In situ monitoring of the BSA/TA coating disintegration (black and red line – 4 BSA/TA bilayers upon the treatment by pH 9 and 11, respectively. Blue - 8 BSA/TA bilayers treated by pH 11. The green line indicates the start of the alkaline treatment.

The spectral shift of resonant wavelength to the initial position after the alkaline treatment of functionalized HC-MOFs indicates the complete removal of BSA/TA films from the capillary walls that has been also verified by SEM micrographs (Figure 7.3a). The stable position of transmission minimum after ~2 min of the treatment at pH 9 suggests completion of the dissolution process. The kinetics of coating removing upon the treatment at pH 11 shows the much faster decay for the coatings with thicknesses of ~20 and ~45 nm (Figure 7.3b). Therefore, a variation in the pH level of the alkaline solution has a strong effect on the kinetics of removing of BSA/TA coating upon the treatment. Thus, the complete removal of the functional layers may vary from a few seconds to a couple of minutes depending on the pH level of the applied solution.

7.3 Summary

To sum up, the proposed technique for the in situ monitoring of LbL assembly of PE multilayers inside the HC-MOFs allows to overcome the current limitations hindering the biomedical applications of optical fiber-based endoscopic probes and sensors. The dynamic measurements based on the tracking of optical resonances enable the noncontact analysis of the adsorption/desorption processes on the fiber surface. As an optofluidic platform, the HC-MOF-based module provides exciting opportunities for fundamental
studies of the LbL process in various types of hollow fibers. Considering the multifunctionality of LbL assembled layers, the designed system offers excellent potential for the development of robust sensors for monitoring both the growth of functional materials and their release under various conditions.
8. Conclusions and future research

In the present thesis, optical properties of hollow-core microstructured fibers modified by polymers and/or inorganic nano- and submicron particles have been studied. Thus, the layer-by-layer modification technique, which has been used to create functional nanocoating in the inner surface of the fiber capillaries, allowed to tune the position of transmission windows in a highly controllable and reproducible way over the broad spectral range from 400 nm to 900 nm introducing an extra attenuation of ~0.02 dB cm$^{-1}$ per single assembled PAH/PSS bilayer. It has been also demonstrated that the thickness and morphology of deposited polymer coating can be controlled through the variation of the salt concentration in the buffer solution. In particular, the average thickness increasing of 1.8 ± 0.3 nm and 7.0 ± 1.3 nm per single PAH/PSS bilayer for the salt-free PE solutions and in the presence of 0.15 M NaCl, respectively, has been observed [14]. Exploiting the set of modified HC-MOFs with slightly shifted transmission windows for the in-fiber multispectral sensing allows the simultaneous measurement of the optical dispersion of biological liquids at many wavelengths in the visible and near-infrared spectral domains. For example, the extraction of the refractive index of bovine serum albumin is possible with refractive index sensitivity values up to ~3000 nm RIU$^{-1}$ and a figure of merit reaching 99 RIU$^{-1}$ [14]. Moreover, the use of the proposed sensing technique has been proved to measure the optical dispersion and concentration of bovine serum albumin dissolved in water and PBS buffers in both static and dynamic regimes, with a resolution of ~1 g L$^{-1}$ [14].

For the first time to our knowledge, the LBL technique for HC-MOF modification through the deposition of silica particles with different sizes (300, 420, and 900 nm) onto capillary surfaces has been presented. The potential for the creation of multilayer porous coating was demonstrated on the example of one, two, and three layers of 300-nm silica particles. The largest spectral shift in the transmission is induced by the first deposited silica layer (31 nm and 39 nm, for the first and the second transmission bands, respectively), while additional silica layers are worse-adsorbed on the first layer of particles, resulting in the additional transmission spectral shifts (11 nm and 7 nm). The limitation of this
technique has been shown in the example of silica particles at the diameters of 900 nm, the bigger particles form the rough coating and disturb the light guidance inside HC-MOFs [94].

The porous silica coatings have been also realized on the sensitive surface of 1D photonic crystal sensors for the creation of functional coatings of different nature: hydrophilic and hydrophobic. Taking into account that condensation in the pores occurs at the lowest partial gas pressures the designed sensor structure shows promising characteristics to detect the changes in surround relative humidity [168].

Ultrasmooth, biocompatible, and removable nanocoating for HC-MOFs has been introduced by BSA/TA complexes. To smooth the BSA/TA substrate, alkaline etching has been applied. The temporal kinetics of the coating dissolution shows that the alkali drops the surface roughness to 3 nm within 4 min of the treatment, resulting in decreasing the fiber optical losses by three times. The coating is fully removed in 7 min of the treatment.
Bibliography


73. E. P. Schartner, G. Tsiminis, A. François, R. Kostecki, S. C. Warren-Smith, L. V.


84. N. Zhang, K. Li, Y. Cui, Z. Wu, P. P. Shum, J. L. Auguste, X. Q. Dinh, G.


111. J. Hiller and M. F. Rubner, "Reversible Molecular Memory and pH-Switchable


137. A. M. Zheltikov, "Colors of thin films, antiresonant phenomena in optical systems,


150. H. G. Tompkins, S. Smith, and D. Convey, "Optimizing the ellipsometric analysis of a transparent layer on glass," Surface and Interface Analysis 29(12), 845–850


X. Zhang, S. Gao, Y. Wang, W. Ding, X. Wang, and P. Wang, "7-cell hollow-core photonic bandgap fiber with broad spectral bandwidth and low loss," Optics Express 27(8), 11608–11616 (2019).


J. K. Lyngsø, B. J. Mangan, C. Jakobsen, and P. J. Roberts, "7-cell core hollow-
core photonic crystal fibers with low loss in the spectral region around 2 μm," Optics Express 17(26), 23468–23473 (2009).
176. N. Sahiner, S. Sagbas, M. Sahiner, C. Silan, N. Aktas, and M. Turk,


